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(71) Applicant and

(72) Inventor: RASMUSSEN, Ole-Bendt [DK/CH]; Sagenstrasse 12, CH-6318 Walchwil (CH).

(74) Agent: GILL JENNINGS & EVERY; Broadgate House, 7 Eldon Street, London EC2M 7LH (GB).

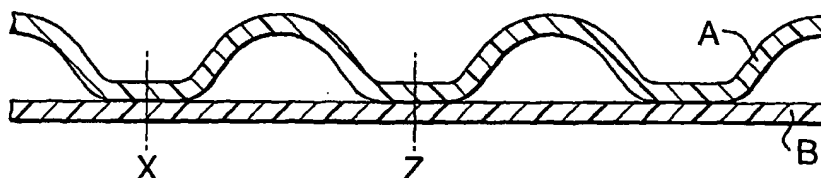
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(54) Title: LAMINATES OF FILMS AND METHODS AND APPARATUS FOR THEIR MANUFACTURE



(57) Abstract: A flexible laminate of films of thermoplastic polymer material comprises fluted ply A and substantially flat ply B, adhered to one another at the crests of A in contact with B. The wavelength of the flutes is preferably no more than 3mm. The thickness of A is generally the same within the non-bonded zones as it is within the bonded zones or A has attenuated zones extending parallel to the flute direction, each bonding zone being mainly located within a first attenuated zone. Apparatus for forming the laminate comprises aligned grooved fluting rollers and grooved laminating roller. The laminate has useful mechanical characteristics, as a flexible material, e.g. when formed into bags which may be self-supporting. Filler material may be filled into the flutes and/or perforations may be provided in one or both plies after lamination.

Laminates of Films and Methods and Apparatus for their  
Manufacture

The present invention relates to a flexible laminate of films from thermoplastic polymer material for applications in which relatively high yield strength and ultimate tensile strength is required, and a method and apparatus for its manufacture.

Examples of such applications are: tarpaulins, pondliners, substitute of geotextiles, weather protective laminates, greenhouse film, industrial bags, carrier bags and self-standing pouches.

For economical reasons there is an increasing need to reduce the thickness or square metre weight of flexible film made from thermoplastic polymer material. The limits are partly set by the required strength properties, and partly by the required self supporting capability, i.e. stiffness with respect to banding. These needs have mainly been met by selected developments of the thermoplastic polymer compositions and as far as the strength is concerned also by biaxial orientation, or by cross-lamination of films each of which exhibits a generally monaxial or unbalanced biaxial orientation.

From strength point of view essential savings can be achieved by such orientation and/or cross-lamination processes.

Thus as an example an industrial bag made from extruded polyethylene film of the best suited grades and destined for packing of 25 kg polyethylene granules must generally have a thickness of 0.12-0.15mm in order to satisfy the normal strength requirements, while this thickness can be brought down to about 0.07mm by use of optimized oriented and cross-laminated film from polyethylene. However, when this cross-laminate is made in the known manner, few available types of machines for manufacturing bags from film, and few available types of machines for filling the bags, can work adequately with film which is so thin and flimsy.

A cross-laminate which, besides the improved strength properties obtained by the orientation and cross-lamination also by virtue of its geometrical structure shows significant improvements in this respect, is described in the inventor's earlier Specification EP-A-0624126.

This is a cross-laminate of a slightly waved configuration in which the material of the curved crests on one or both sides of the laminate is thicker than elsewhere, the material between these thicker curved crests being generally straightened out. (See Figs. 1 and 2 of said patent publications.) The structure is obtained by stretching between several sets of grooved rollers under special conditions. This stretching also imparts transverse orientation. The disclosed wavelengths of the final products are between 2.2 and 3.1mm.

Cross-laminates according to the said patent have been produced industrially since 1995 for manufacture of industrial bags from combinations of high molecular weight high density polyethylene (HMWHDPE) and linear low density polyethylene (LLDPE) with film weight about  $90 \text{ gm}^{-2}$ , and the slightly waved shape in combination with the thickened crests imparts a stiffness in one direction of the film which has proven to be very important for the performance of the bag machines with such relatively thin film. However, the film is not adequate for work with the  $70 \text{ gm}^{-2}$  gauge which satisfies the strength requirements.

Furthermore the corrugated character of the film surface makes a particularly fine print (as often required) impossible and also to some extent reduces the friction between filled bags in a stack, when the layers of this stack are built up with the bags in crisscrossing arrangement as usually done.

As another example an agricultural tarpaulin (e.g. for protection of crops) made from a  $70 \text{ gm}^{-2}$  cross-laminate of oriented polyethylene films would be a fully adequate substitute of a  $100 \text{ gm}^{-2}$  tarpaulin made from extrusion-coated woven tape, if only objective criteria were applied.

However, in actual fact the average customer to agricultural tarpaulins makes his choice to a great extent on the basis of the "handle" and the appearance, and will reject the 70 gm<sup>-2</sup> tarpaulin due to its flimsiness, judging  
5 that it lacks substance.

The stiffness can of course always be increased by suitable incorporation of a filler, (and the present invention includes that as an additional option) but this will always more or less be at the expense of puncture and  
10 tear propagation resistance, especially under impact actions.

Object of the present invention is to add a "feel of substance" and improve stiffness in laminates of films at least in one direction, without sacrificing the laminate's  
15 character of feeling and looking like a generally two-dimensional structure, furthermore without essentially harming the puncture and tear propagation resistance, and when desired also providing a good printability at least on one side of the laminate.

The basic idea behind the present invention is to apply the corrugated paperboard principle to laminates of thermoplastic films, but in such a way that the flute structure is made extraordinarily fine ("minifluted"), so as to obtain a laminate which, in spite of the structurally  
20 increased stiffness (at least in one direction), can still satisfy the above-mentioned conditions.

In itself the application of the corrugated paperboard principle to the thermoplastic film is not new, but the finest flute structure which has been disclosed in patent  
30 literature, namely in US-A-4132581 col. 6, ln. 66, is 50+/-3 flutes per foot corresponding to a wavelength of about 6.0mm. It must also strongly be doubted that a wavelength lower than this can be achieved by the method disclosed in the said patent, in which the first bonding process takes  
35 place under use of a row of many sealer bars supported and transported by a belt.

The sealer bars are transverse to the direction of movement (the machine direction) so the fluting also becomes perpendicular to this direction.

The use of the method of the said US patent is stated to be manufacture of board material, and the thickness of the fluted ply is indicated to be about 0.004-0.025 inches (0.10-0.625mm). In the example it is 0.018 inches (0.45mm). Other patents dealing with the use of the corrugated paperboard principle to thermoplastic film for the making of panels or boards are US-A-3682736, US-A-3833440, US-A-3837973, EP-A-0325780 and WO-A-94/05498.

Japanese Patent Application Hei 02-052732 discloses laminates consisting of a corrugated thermoplastic film bonded to a flat thermoplastic film, which on its other side is bonded to paper. (The paper and flat sheet are first joined and then the corrugated film is added.) The flutes, which also in this case are perpendicular to the machine direction are pressed flat and adhesively closed at intervals so that a large number of airtight vesicles are formed. The stated use of this product is for cushion material, sound insulating material, heat- and moisture-insulating material and wall decorative material. The thickness of the corrugated sheet and flat sheet are not indicated, neither are the wavelength of the fluting and the length of the vesicles, but it is mentioned that the dimensions can be selected depending on the use of the laminate. However, it must be understood as implied that the wavelength in any case will be no lower than the lowest mentioned in the above-mentioned US-A-4132581 (i.e. about 6mm). One reason for judging this is that this would not be advantageous for the mentioned purposes, except for decoration, while another reason is that the disclosed apparatus would not be able to work with a lower wavelength (i.e. a lower pitch of the gear rollers) except for making an extremely shallow and practically useless fluting. This is due to the fact that thermoplastic film is resilient and not permanently formable at ambient temperature which as

implied by the presentation in the drawing is used in the said method. If the pitch is low on the gear rollers which produce the fluting and the lamination, the corrugated film will "jump out" of the grooves in the forming and laminating roller during its passage from the location where forming of flutes takes place to the location where bonding takes place. The patent publication does not mention any means to hold the flutes in shape in the grooves of the roller.

10 In a conventional corrugator for manufacture of corrugated paperboard there are provided tracks or shield to hold the fluted paper in the grooves. At ambient temperature this allows the paper to be more readily permanently formed.

15 Similar tracks or shields in unmodified form cannot be used with thermoplastic film under production conditions since friction against the track or shield quickly would create congestion by heating of the polymer.

20 An improved, frictionless way of holding of flutes of paper in the grooves of a roller is known from US-A-6139938, namely by maintaining a controlled under pressure within the grooves (see Figs. 9 and 10 and col. 7 lines 25-34). This US patent deals entirely with corrugated paper laminates having particularly low wavelength while manufacture of corrugated structures from thermoplastic films is not mentioned. However, the improved method of holding the flutes will in fact also, depending on the film thickness, be applicable to fine flutes in thermoplastic film. This was found in connection with the development of the present invention. However as mentioned above, the Japanese patent application does not disclose any precautions to hold the flutes in shape in the grooves.

30 The development of the particularly fine flute structure, the "miniflutes", which is the object of the present invention has made the corrugated paperboard principle applicable to completely different fields of use

such as the fields mentioned at the very beginning of this specification.

This has comprised a development of new types of machinery based on grooved rollers with a very fine pitch.  
5 As it will appear from the example the wavelength in a 90  $\text{gm}^{-2}$  "minifluted" 2-ply laminate (each ply about 45  $\text{gm}^{-2}$ ) has in actual fact been brought down to 1.0mm through a process which can be carried out industrially, and after shrinkage of the flat ply transversely to the flutes it has  
10 even been brought down to 0.8mm. Especially by further use of shrinkage it can probably be brought further down e.g. to about 0.5mm. The mentioned 2 x 45  $\text{gm}^{-2}$  corresponds to an average thickness of about 0.074mm (2x0.037mm) if the laminate were pressed flat.

15 The invention is not limited to pressed-flat thicknesses around this value, but also comprises, very generally speaking, minifluted laminates of an average thickness in compacted form which is roughly about 0.3mm or lower. Thicknesses down to 0.03mm or even lower can be  
20 made for special purposes.

Nor is the invention limited to the use in connection with cross-laminates of oriented films. For different purposes different combinations of strength properties are required. Cross-laminates can, as is known, be produced  
25 with suitable combinations of several categories of strength properties but for many purposes other types of strength laminates may be preferable when the cost of the manufacturing process also is considered, and the present invention can also be useful in such other strength  
30 laminates as it further shall be specified below.

By making the wavelength as low as 3mm or less, the laminate loses its character of being a board material and gets appearance, handle and bending properties like a flexible film (see the example). It also gets improved  
35 puncture properties, compared to laminates made from similar plies but with longer wavelength, since in the latter there is a large tendency for the plies to be

ruptured individually instead of cooperating in the resistance against the puncture.

The "minifluted" laminate also has the advantage that it can receive a fine print on the flat side and a coarse  
5 print on the corrugated side.

Compared to non-corrugated laminates of the same composition and same square metre weight it feels much more substantial due to the increased stiffness in one direction and due to the increased volume.

10 In the case of cross-laminates it is well-known that a weak bonding between the plies, or strong bonding or line-bonding, gives much improved tear propagation resistance, since it allows the tear to proceed in different directions in the different plies. Thereby the  
15 notch effect is reduced. Since a cross-laminate with one ply corrugated will be line-bonded, it will show improved tear propagation resistance, no matter whether the wavelength is short or long, however "mini-fluting" makes the tear stop after a very short propagation, which of  
20 course is very advantageous in most cases.

For the sake of good order, it should be mentioned that there already have been described "minifluted" laminates in literature, however laminates of which at least the fluted ply consists of a material which is not a  
25 thermoplastic film or an assembly of thermoplastic films.

Thus US-A-6139938, which has been mentioned above, has for its object a 3-ply paper laminate with a corrugated paper sheet in the middle and flat paper sheets on each side, like normal corrugated paper board, however claimed  
30 to comprise 500-600 flutes per metre corresponding to a wavelength of 1.67-2.00mm. This state purpose is to improve the printability.

Japanese patent publication No. 07-251004 relates to an absorbing product in which a plane thermoplastic  
35 synthetic fiber sheet is thermally bonded to a corrugated sheet mainly consisting of active carbon fibers. The wavelength of the corrugation is 2.5-20mm.



Japanese patent publication No. 08-299385 relates to an absorbent laminate consisting of a fluted non-woven fabric bonded on one side to a plane sheet or film, which can be a thermoplastic film. Between these two plies there is nested a water-absorbing material. The wavelength is claimed to be 3-50mm, and it is stated that there would not be sufficient space for the absorbing material if it were less. The product is for diapers and the similar products.

More precisely expressed the present invention concerns a laminate comprising at least a monofilm-formed or multifolded ply (A) and another monofilm-formed or multifolded ply (B) both mainly consisting of thermoplastic polymer material, whereby at least A consists of cold-orientable material in which A has a waved flute configuration while B is not waved, and B on a first side is adhesively bonded in bonding zones to the crests on a first side of A. A characterising feature of the laminate is that the wavelength of the said configuration is no more than 3mm. The use of cold-orientable material in A is important for the strength of the product. Furthermore it is normally important that the adhesive bonding has been established through a lamination layer, so that melting of the main portions of A and B can be avoided during the lamination process, and that either the thickness of A generally is the same within the non-bonded zones as it is within the bonded zones, or A exhibits zones which are attenuated in the solid state and extend parallel to the flute direction in such a manner that each bonding zone mainly is located within one of the attenuated zones. These attenuated zones will be referred to as the "first attenuated zones" since there also may be further attenuated zones, as it shall be explained later.

In this connection, an essential attenuation of A in the non-bonded zones, as compared to the thickness of A in the bonded zones, will of course have a negative influence on the resistance to bending in the stiff direction (but it is generally easier to make the fluted laminate so). By

contrast this resistance to bending is enhanced, seen in relation to the average thickness of ply A, when each bonding zone mainly falls within one of these attenuated zones. The attenuated zones also facilitate the manufacturing process as it later shall be explained. It is noted that while attenuation by stretching in the molten state reduces the tensile strength, attenuation by stretching in solid state increases the tensile strength in the direction in which this stretching has taken place.

While I here have identified the laminate as comprising the plies A and B, each "ply" can consist of one or more "films", normally extruded films, and each extruded film can and normally will consist of several co-extruded "layers". Thus the "lamination layer" through which the bonding takes place will normally be a co-extruded layer, however it can also be a thin film applied in a conventional extrusion-lamination process.

While an upper limit of 3mm wavelength has been chosen as a suitable value for distinguishing the product of the invention from corrugated board material, it is generally better to keep the wavelength within 2.5mm, preferably within 2 mm and more preferably 1.5mm. As already mentioned and shown in the example the inventor has been able to make it 1.0mm and under use of shrinkage after lamination even 0.8mm.

As it appears from the introduction, the use of the present invention is mainly for strength film. This needs not always mean good strength in all directions; by contrast there are cases, e.g. in construction of bags, where the focus should be on the strength in one direction, combined with a certain puncture and tear-propagation resistance. As an example a conventional industrial bag of film thickness 0.160mm made from a blend of 90% LDPE and 10% LLDPE will typically in its longitudinal direction show a yield force of  $20 \text{ Ncm}^{-1}$ , i.e. a yield tension of 12.5 MPa and in its transverse direction shows a yield force of  $16 \text{ Ncm}^{-1}$ , i.e. a yield tension of 10.0 MPa.

Cross-laminated film material in average thickness 0.086mm for heat-sealable bags developed by the inventor and manufactured in accordance with the above-mentioned EP-A-0624126 shows in its strongest direction a yield force of  
5 20 Ncm<sup>-1</sup>, i.e. 23 MPa, and in its weakest direction a yield force of 17 Ncm<sup>-1</sup>, i.e. a yield tension of 20 MPa.

Since the invention in principle relates to flexible laminates for uses where relatively high strength is required, although the emphasis of the invention is on  
10 stiffness, feel and appearance, the yield tension of the laminate in its strongest direction should normally be no less than 15 MPa, preferably no less than 25 MPa. Correspondingly the ultimate tensile tension is conveniently about twice the said indicated values, or  
15 more. Here the cross section in mm<sup>2</sup> is based on the solid material only, not including the air spaces, and it is an average, considering that ply A may have attenuated zones.

The yield tensions mentioned here refer to tensile testing at an extension velocity of 500% per minute. They  
20 are established from strain/stress graphs. These graphs will begin linear accordingly to Hook's law, but will normally soon deviate from linearity although the deformation still is elastic. In principle the yield tension should be the tension at which the deformation  
25 becomes permanent, but this critical value, which is velocity dependent, is practically impossible to determine. The way yield tension normally is determined in practice, and also considered determined in connection with the present invention, is the following:

30 In case the tension reaches a relative maximum, then remains constant or decreases under continued elongation, later to increase again until break occurs, the relative maximum of the tension is considered to be the yield tension. The sample may also break at this point, and then  
35 the yield tension equals the ultimate tensile tension. If however the tension continues to increase with the continued elongation, but with much lower increases in

tension per percentage elongation, then the strain/stress curve after yield, and after it practically has become a straight line, is extrapolated backward to intersect with the line which represents the Hook's-Law-part of the stretching. The tension at the intersection between the two lines is the defined yield tension.

An embodiment of the invention is characterised in that the ply A by the choice of polymer material or by an incorporated filler or by orientation, within the non-bonded zones exhibits an average yield tension parallel to the direction of fluting, which when it is determined as explained above, is no less than  $30 \text{ Nmm}^{-2}$  (cross-section of ply A alone), preferably no less than  $50 \text{ Nmm}^{-2}$  and still more preferably no less than  $75 \text{ Nmm}^{-2}$ .

As already mentioned, A is preferably solid-state-attenuated in zones (the "first attenuated zones") and each bonding zone is mainly located within a first attenuated zone. These zones should be understood as delimited by the positions where the thickness of A is an average between A's lowest thickness within the first attenuated zone and A's highest thickness within the adjacent non-bonded zone.

Another important embodiment of the invention is characterised in that A within each non-bonded zone and outside the first attenuated zone if such zone is present (delimited as mentioned above) is molecularly oriented mainly in a direction parallel to the direction of the flutes or a direction close to the latter as established by shrinkage tests. Such tests are commonly used. In this connection, a component of orientation in A perpendicular to the direction of the flutes will not contribute to the yield tension in any direction, but will contribute to certain other strength properties.

A preferable limitation of the extension of each first attenuated zone - preferable with a view to the stiffness in one direction - is specified in claim 12, and preferable thicknesses of these zones are specified in claim 21.

Additionally to the first attenuated zones it can be very advantageous to have a second solid-state-attenuated zone (hereinafter the second attenuated zone) between each pair of adjacent first attenuated zones. These second  
5 attenuated zones should be narrower than the first ones - preferably as narrow as possible but also alternated so that the thickness of A in the zone is as thin as possible - and located on the crests of A on the side opposite to the bonded zones. They act as "hinges", and if they are  
10 made narrow and deep enough they improve the stiffness since the cross-section of A becomes zig-zagging instead of smoothly waved (as described further in connection with Figure 3) and A and B thereby form triangular structures. They also essentially facilitate the manufacturing process,  
15 which is explained below.

In addition to the improvements in stiffness caused by the first and second attenuated zones (improvements seen in relation to the average thickness of A) each set of zones also normally improves the resistance against shock  
20 actions, i.e. they normally improve impact strength, shock-puncture resistance and shock-tear-propagation resistance. This is because there is started a stretching (or further stretching if A already was stretched) and this stretching normally has a tendency to progress under shock actions,  
25 whereby the first and second attenuated zones can act as shock-absorbers.

Normally the wavelength of each flute including an adjacent bonding zone should be no longer than 50 times the highest thickness of A within the flute, preferably no more  
30 than 40 times and still more preferably no more than 30 times the said thickness. As an example, if the highest thickness of A is 0.037mm as in the operative example below, the mentioned values correspond to wavelengths of 1.85, 1.48 and 1.11mm respectively.

35 In order to "integrate" the plies conveniently with each other in order for strength purposes, the width of each bonding zone should normally be no less than 15%,

preferably no less than 20% and still more preferably no less than 30% of the wavelength, and in order to achieve a substantial effect of the fluting, the width of each non-bonded zone of A as measured between the two adjacent bonding zones and measured along its curved surface, should preferably be no less than 10% and preferably no less than 20% longer than the corresponding linear distance. This is a measure of the depth of the flutes.

For many purposes, e.g. when increased stiffness against bending in all directions is wanted, there can be a non-waved monolayered or multilayered film C on the side of A which is opposite to B as specified in claim 15.

A fluted outside surface on a bag has as mentioned above a disadvantage, namely in connection with printing and stacking of the filled bag. However there are articles in which the special roughness of a fluted surface can be very advantageous in use e.g. on mats. For such articles there can advantageously be two waved mono- or multilayered plies (A) and (D) laminated to the two opposing sides of the non-waved mono- or multilayered film (B), as specified in claim 16.

The films A, B, C and D will normally consist of polyolefin and will normally be produced by a process which involves extrusion. This will normally be a co-extrusion process by which lamination layers and optionally heat-seal layers are joined with the main body of the film.

At least some of the flutes can be flattened at longitudinally spaced intervals and preferably bonded across the entire width of each flute at the flattened locations to make the flutes form a row of narrow closed elongated pockets. Preferably the flattened portions of a number of mutually adjacent flutes or of all flutes form a series of lines transverse to the longitudinal direction of the flutes. This can make the corrugated laminate look and feel more textile-like, almost make the impression of a woven structure, and make it more flexible in the direction which otherwise is stiff, without losing the feel of bulk

and substance. Flattening can also be used to create preferential locations for bending.

Further description of different embodiments of the product and of particular uses will follow after the  
5 description of the method.

In accordance which the above characterization of the laminate of the invention, the method of manufacture which takes place under use of a grooved roller for formation of the flutes, and also under use of a grooved roller for the  
10 lamination by heat and pressure (which in certain cases can be the same grooved roller) is characterised in that the division on the roller which produces the lamination is at the highest 3mm. The new method according to the invention is as defined in claim 36. New apparatus suitable for  
15 carrying out the method is defined in claim 65.

The apparatus can be adapted either to make the flutes generally perpendicular to the machine direction as in conventional manufacture of corrugated laminates, or generally parallel to the machine direction. This will be  
20 specified below.

Normally the bonding is established through a lamination layer (produced by co-extrusion or by an extrusion lamination technique) in order to avoid weakening, and normally the steps of the process are  
25 adapted either to avoid any significant attenuation of the zones in A, or alternatively a stretching in solid state between a set of grooved rollers is adapted to produce the above-mentioned "first attenuated zones", whereby the grooved roller for lamination is coordinated with the set  
30 of grooved rollers for stretching in such a way that each zone of bonding mainly becomes located within a first attenuated zone.

The "second attenuated zones", which have been described above in the description of the product, can be  
35 formed by stretching between a further set of grooved rollers suitably coordinated with the grooved rollers which produce the first attenuated zones.

The advantages of the first and second attenuated zones in terms of product properties have already been explained. For the carrying out of the method, the first attenuated lines allow increases of velocity and therefore improved economy, since the zones in ply A which are going to be bonded, have been made thinner and therefore require less heating time during the application of heat prior to the bonding. Furthermore the first attenuated zones and in particular the combination of first and second attenuated zones can be of great help for the process by acting as "hinges" in ply A. In the type of apparatus in which the grooved roller for lamination has grooves which are generally parallel with its axis, these "hinges" make it possible to direct even relatively heavy A-ply into fine grooves. In the type of apparatus in which the grooves are circular or helical, but in any case approximately perpendicular to the roller axis, the "hinges" help to keep ply A "in track" during its passage from grooved roller to grooved roller, in other works the "hinges" help to coordinate the action of the grooved lamination roller with the action of the preceding set or sets of grooved rollers which form the flute under a simultaneous transverse stretching.

While it is essential for normal uses of the invention for applications as a flexible film that the division on the grooved roller which produces the lamination on the crests is no more than 3mm, it is generally recommendable to make it no more than 2.5mm, preferably no more than 2.0mm and still more preferably no more than 1.5mm.

The film or films used for ply A is preferably, prior to forming of the waved configuration and prior to making of the first and second attenuated zones (if such zones are made), supplied with orientation in one or both directions, the resultant main direction of orientation being in the direction which is selected to become the direction of fluting. This can be by means of a strong melt orientation, or preferably, alternatively or additionally



by known stretching procedures carried out in the solid state. If the process is adapted to make the flutes generally parallel with the machine direction, this will be a generally longitudinal orientation process, which is  
5 simple, and if the process is adapted to make the flutes generally perpendicular to the machine direction, it will be a generally transverse orientation process which is much more complicated to establish and usually requires expensive machinery. It is noted that neither of the two  
10 closest references, i.e. US-A-4132581 and Japanese patent application Hei 02-052732 have disclosures which indicate that ply A could be oriented in a direction generally parallel with the flutes. In these two publications the flutes are formed in the transverse direction, and had  
15 there been thought of using transversely oriented film it would have been natural to mention this, since without special steps the film is not formed so in the extrusion or casting process.

As it already has been described in connection with  
20 the product, a further non-waved monofilm formed or multifilm formed ply (C) of thermoplastic polymer material can simultaneously with or subsequent to the bonding of B to A be adhesively bonded to the crests of A on the second side of A. Another useful possibility is that, in a manner  
25 similar to the forming and application of A, there is produced a second monofilm formed or multifilm formed ply (D) having waved flute configuration with a wavelength of preferably no more than 3mm, and the crests on one side of D are laminated to the second side of B simultaneously with  
30 or following the lamination of B with A.

In most applications of the invention the mono- or multifilm formed plies should mainly consist of polyolefin, and should be produced by a process involving extrusion. Furthermore the films constituting the plies should  
35 normally be made by co-extrusion in which there is co-extruded surface layers to enable the lamination without any melting of the main body of the films.

As it also appears from the description of the product, some of the flutes at least can be flattened after the lamination. This is done at intervals, preferably under heat and pressure sufficient to bond all films in the laminate to each other so that the flutes with adjacent film material form fine elongated pockets closed at each end. The flattening can be carried out with bars or cogs which have their longitudinal direction arranged transversely to the flute direction and which each covers a number of flutes, optionally the entire width of the laminate.

A suitably distinct formation of the first attenuated zones can be established at least in part by giving the crests on the grooved stretching roller intended to produce the stripes a temperature which is higher than the temperature of the crests on the other grooved stretching roller and/or by giving the crests on the grooved stretching roller intended to produce the stripes a radius of curvature which is smaller than the radius of curvature of the crests on the matching grooved stretching roller. A significant orientation mainly in the direction nearly parallel with the fluting, and/or a high co-efficient of elasticity (B) of ply A are also efficient means to give the first attenuated zones suitably distinct borders.

A good way to make the fluting finer than this can be done by purely mechanical means is by use of shrinkage. Prior to the lamination ply B is supplied with orientation generally perpendicular to the direction which becomes direction of fluting, and after the lamination B is subjected to shrinkage in a direction generally perpendicular to the direction of fluting.

As it already has been stated the waved flute structure can be formed in different directions. Thus it can be established mainly in A's longitudinal direction under a generally transverse orientation process by taking A through a set of driven mutually intermeshing grooved rollers, the grooves of the rollers being circular or being

helical and forming an angle of at least 60° with the roller axis. It is most practical to make this angle about 90° or at least very close to this. This can be arranged so that A moves directly from its exit from one of the grooved stretching rollers which form the waving on A to the grooved lamination roller, whereby these two grooved rollers are in close proximity to each other and have the same pitch, and are mutually adjusted in the axial direction. The pitch, in this aspect should be measured at the operational temperature of the respective roller.

Alternatively A can move from this exit from one of the grooved stretching rollers which form the waving on A to the grooved lamination roller over one or a series of heated, grooved transfer rollers. The grooved rollers in this row start with the grooved stretching rollers and end with the grooved lamination roller and each is in close proximity to its neighbour or neighbours. Each of the grooved rollers in the row has the same pitch (measured at the operational temperature of the respective roller) and their axial positions are adjustable to each other (see figs. 7 and 8 and the example).

When the fluting is produced in the longitudinal direction by means of rollers with circular grooves, ply A's width measured as the direct, linear distance will remain constant from its inlet to the process of the lamination, apart from deviations in very narrow edge regions, which should be trimmed off. Therefore, the ratio between ply A's real width, measured along its curved extension, and A's linear width, which is the same as B's width, equals the transverse stretch ratio and is related to the thickness reductions in the attenuated zones.

However, as it already has been mentioned, the flutes can also be produced in a distinctly transverse direction. In this embodiment, an angle of about 30° between the grooves and the roller axis is probably about the maximum which is practically possible, but it is simplest to work with grooves which are parallel with the roller axis.

The embodiment with grooves parallel to the roller axis is further defined in claims 56, 57, 58 and 59. The means to hold A in fluted form in the grooves from flute formation to bonding, and adapted to avoid a frictional rubbing on A, can be devices for suction through channels from the inside of the grooved roller - a method which as already mentioned is known from making of corrugated paperboard - or it can be use of tracks or shields which are adapted from the constructions used in manufacture or corrugated paperboard by being air-lubricated. This means that the tracks or shields are supplied with fine channels, or preferably a part of each track or shield is made from porous, sintered metal, and pressurized air is blown through the channels or pores to form an air-film on which the fluted ply can flow.

The means for fine regulation mentioned in claims 58 and 59 are similar to registration means in multicolour printing technology.

The following sections will describe different selections of the orientation and/or elasticity in the different plies, special utilization of the channels or pockets formed by the flutes, and particular end uses of the product of the invention.

It has already been mentioned that, in an important embodiment of the product according to the invention, ply A within each non-bonded zone and outside the first attenuated zone if such zone is present, is molecularly oriented mainly in a direction parallel to the direction of the flutes or a direction close to the latter.

With ply A so oriented, there are different preferable options for ply B, depending on the uses of the laminate. One very important option is that B also is molecularly oriented and B's orientation within each non-bonded zone in a direction perpendicular to the direction of the flutes is higher than A's average orientation in the same direction within the non-bonded zone. The said two components of

orientation are also in this case, indicated by shrinkage tests.

This does not necessarily mean that ply B must have its strongest component of orientation in the transverse direction, in other words the laminate needs not necessarily be a cross-laminate. Thus, ply B may simply be a highly blown film, which by means of the high blow ratio has obtained a relatively high transverse melt orientation. The embodiment is further specified in claim 8.

As mentioned there are cases, e.g. in bag construction, in which there is a need for a high yield tension in one direction only, but combined with high puncture resistance. The laminate according to claim 9 or claim 10 is designed for this.

As it appears from the foregoing the present invention is very useful in connection with cross-laminates, i.e. the laminate then comprises at least two films each of which has a main direction of orientation and which are laminated so that the said two directions cross each other. Different ways of carrying out this aspect of the inventions appears from product claims 22 to 25, from which also the method of making becomes clear.

Suitable methods and apparatus for cross-lamination may be achieved by combining the information in the above mentioned EP-A-0624126, mainly in its introduction, with the formation in the inventor's older GB-A-1526722. Thus, with reference to Fig. 4 of the present drawings, B and C may each be films, including laminates, which exhibit a main direction of orientation whereby B's main direction of orientation criss-crosses with C's main direction of orientation. One of these directions may be parallel with the machine direction, the other perpendicular thereto, or both may form an angle higher than 0° and lower than 90°, preferably between 20° and 70° and more preferably in the range 25° - 65° with the machine direction. In this arrangement the waved A supplies to the laminate stiffness against bending, but at the same time, since it establishes

a "dislocated" bonding between B and C, it also has importance for the tear propagation resistance. It is known e.g. from the above-mentioned GB-A-1526722, that the superior tear propagation resistance which can be obtained  
5 by cross-lamination, depends on having bonding strength which is not too high, since the tear must be allowed to develop along different directions in the different plies of the cross-laminate. Since on the other hand the cross-laminate should not be prone to accidental delamination  
10 during use, as for instance described in the said patent, there can be used a combination of strong bonding in spots or lines and a weak bonding over the rest. However, the "dislocated" bonding of cross-laminated B and C through the waved A can provide a better combination of high tear  
15 propagation resistance and adequate bonding strength, especially when the coefficient of elasticity E of film A is lower than the coefficient E for both B and C, preferably by a factor of at least 1.5 and more preferably at least 2. Furthermore the flutes may be flattened at  
20 intervals and bonded across each ones entire width to make the flute from a row of narrow, closed pockets. The purposes of such flattening have been mentioned above.

In the above description there is mentioned the "main direction of orientation" in the films B and C. If plies  
25 B and C each are mono-films, normally with coextruded surface layers, this may be a monoaxial or unbalanced biaxial orientation. However, each of the films B and C may also in themselves be cross-laminates, normally 2-ply cross-laminates.

30 To clarify this, B may e.g. consist of two plies of equal composition, equal thickness and equal degree of orientation, but one oriented at  $+30^\circ$  and the other at  $-30^\circ$  to the machine direction. This will result in a main direction of orientation following the machine direction.  
35 Similarly C may consist of two equal plies, one oriented at  $+60^\circ$  and the other at  $-60^\circ$ . The resultant direction of orientation then is perpendicular to the machine direction.

Uniaxial or unbalanced orientation in a film can be obtained under use of spiral cutting of a tubular film with mainly longitudinal direction as disclosed in EP-A-0624126 and GB-A-1526722, both mentioned above, and disclosed in  
5 more detail in EP-A-0426702. The latter also discloses a method of obtaining a uniaxial or strongly unbalanced melt-orientation which is perpendicular to the machine direction, namely by twisting of a tubular film coming out of the extrusion die followed by helical cutting under the  
10 calculated angle. Another embodiment of the cross-lamination aspect of the present invention is stated in claim 22. The expression "resultant main direction of orientation" has the same meaning as explained above.

If this laminate is to be used in the construction of  
15 bags with heat-seals generally perpendicular to the direction of the flutes, and if such heat-seals may be subjected to high shock-peel forces then the laminate should preferably be constructed as stated in claim 61. The fluted softer A-film can then form the inner side for  
20 heat-sealing, and the stiffer, smooth B-film can form the outer side of the bag.

Another aspect of the invention ("the encapsulation/canalization aspect") comprises a number of embodiments which for different practical purposes utilize  
25 the interior cavities in the laminate, optionally in combination with suitable perforations, either to canalize a flow of liquid or air, or to encapsulate filling material in particulate, fibrous, filament or liquid form. The latter may e.g. be a preservative for goods packed in the  
30 flexible laminate. These different embodiments appear from product claims 27 to 30, 34 and 35. The method of making these products will appear from claims 48 to 51, and apparatus suitable for carrying out the method is defined in claims 88 and 89.

35 The embodiment of the present invention in which the fine canals or "pockets" are used to "bury" preservatives, have obvious advantages over the usual method of blending

such agents with the polymers to be extruded into film form. One advantage is that the concentration of the preservative can be much higher, another that the preservative needs not be able to withstand the temperature of extrusion. The preservative may reach the object to be preserved by migration alone, or if the agent is solid it may gradually evaporate and diffuse through sufficiently fine perforations or pores.

It is also customary to contain preservative agents in small bags which are placed inside a package. Compared to this method of protection, the present invention has the advantage that the preservative agent can be distributed almost homogeneously over the full area of the packing material.

The filter material stated in claim 30 has many potential uses, e.g. as a geotextile (claims 34 and 35) but also for instance for water treatment in the chemical industry and in gas face masks.

Although the claims relating to these filter materials, including the weather-protective laminate of claim 62, formally depend on claim 1, it should be understood that similar products having wavelength somewhat higher than 3mm also have important uses and are considered inventive new products. Thus in a further aspect of the invention there is provided a laminate comprising at least a monofilm formed or multifilm formed ply (A) and another monofilm formed or multifilm formed ply (B) both mainly consisting of thermoplastic polymer material, whereby at least A consists of cold-orientable material in which A has a waved flute configuration while B is not waved, and B on a first side is adhesively bonded in bonding zones to the crests on a first side of A in which the adhesive bonding has been established through a lamination layer, and that either the thickness of A is generally the same within the non-bonded zones as it is within the bonded zones, or A exhibits first solid-state-attenuated zones (hereinafter the first attenuated zones) extending parallel to the flute



direction, each bonding zone mainly being located within a first attenuated zone, the laminate being moisture resistant but air permeable. The laminates are useful for forming raincoats and tarpaulins. Other uses in which an additive is incorporated into the flutes are described below.

Other important uses of the invention are for bags and self-standing pouches. In this connection reference is made to the product claims 31, 32 and 33.

For all uses of the present invention, a very interesting and wear-resistant print can be obtained when, prior to the lamination, A and/or B is supplied with print on the surface to become the inside of the laminate, the printing process being in register with the flute-forming and lamination processes so as to limit the print generally to the non-bonded zones. This durable print may form a text, a decorative pattern or simply lines which accentuate the fluting or the textile-like appearance of the laminate. Special decorative effects can be achieved if the print provides a metallic appearance or a mother-of-pearl effect.

The invention shall now be explained in further detail with references to the drawings.

Figs. 1, 2, 3, 4 and 5 are cross-sections representing four different structures of the laminate of the invention, comprising the minifluted ply A, or plies A and D, and the straight ply B or plies B and C. The flutes in each of these structures can extend longitudinally or transversely, seen in relation to the machine direction of the flute-forming and laminating machinery.

Fig. 6 is an enlarged detail of Fig. 1 to illustrate how these plies themselves can be laminates of films, and how these films can be multilayered as made by co-extrusion, this being done to facilitate bonding and lamination.

Fig. 7 is a principal sketch representing the steps from formation of the miniflutes in A to lamination of A with B in the manufacture of the product shown in Fig. 2,

the different steps being represented by the cross-sections of the films A and B and by the cross-sections through the axis of the rollers of the surfaces of the rollers.

Fig. 8 is a sketch of the machine line corresponding to Fig. 7 with addition of the means to laminate straight film C to A opposite to B.

Figs. 9a, 9b and 9c are sketches illustrating the cross-laminate constructed as stated in claim 22.

Figs. 10a, b and c represent sections parallel to the flutes and through the middle of a non-bonded zone, showing applications of the invention in which the channels or pockets formed between ply A and ply B are used as mini-containers or to canalize a flow of air or water, namely in fig. 10a as mini-containers for a protective agent, in Fig. 10b for filtration and in Fig. 10c for weather protection.

Fig. 11 shows a modification of the lamination station of Fig. 8 in which there are added filling devices to fill particulate material into the flutes before the lamination, and added sealing equipment to form transverse seals after the lamination, thereby making closed pockets which serve as "mini-containers" for the particulate material.

Fig. 12 is a flow-sheet showing a process for producing the laminate with transverse fluting and with "first" and "second" attenuated zones (as these expressions have been defined).

Fig.13 shows a detail of a grooved lamination roller for formation of transverse fluting, air jets being used to direct the ply into the grooves and vacuum being used to retain it there.

With references to Figs. 1 to 5 it should be mentioned for the sake of clarity, that the wavelength referred to in the foregoing and in the claims, is the straight linear distance from x to z. This distance is preferably 3 mm or lower, and as it appears from the example, the inventor has been able to make it as small as 0.8mm, which however needs not be the ultimate lower limit obtainable and useful. It is noted that US-A-5441691 (Dobrin et al.) makes embossed

film (not heat-bonded laminates) having a generally circular shape of the bosses, with a spacing from centre to centre which can be still finer than these 0.8mm, however the bosses of this patent are drawn much thinner than the main body of the film.

In Fig. 1 the thickness of ply A is generally the same across the ply. In case of transverse fluting this can be achieved by the process shown in Fig. 12 (without preceding formation of attenuated zones) however there is a limit, which is of practical importance, of how fine the wavelength can be, seen in relation to the thickness of ply A.

In case the flutes are made parallel with the machine direction, for formation of the flutes and the lamination is preferably carried out generally as shown in Fig. 8. This means there will always be a transverse stretching between intermeshing grooved rollers, and the degree of fluting will correspond to the degree of stretching. When film is stretched between very fine grooved rollers, there will be a strong tendency to localize the stretching entirely or predominately on and near to the tips of the grooves. This can be avoided, but with difficulty, by using film which in a preceding process has been transversely stretched, and feeding the film unto the roller at a temperature which is higher than the temperature of the roller.

However, in the laminate structures shown in Figs. 2 to 5 the differences of thickness resulting from grooved roller stretching has been utilized in a way which generally is an advantage for the properties of the product. By the exact registration between the grooved rollers for stretching, the grooved roller for lamination and a grooved transfer roller therebetween, it is arranged that each bonding zone mainly falls within an attenuated zone. As it appears from Fig. 3 there can be two sets of attenuated zones for each zone of bonding, namely a series (6) of wider ones ("the first attenuated zones") within

which the bonding zones fall, and a set of shorter ones (101), the latter referred to as the "second attenuated zones".

By attenuating ply A at the basis where it is bonded  
5 to ply B, the thickness of A is minimized at the location where its contribution to stiffness in the stiff direction in any case is insignificant. By introducing the narrow "second attenuated zones" which act as "hinges", the cross-section becomes almost triangular as shown in Fig. 3. This  
10 means that the stiffness is further improved. These attenuated zones also introduce a tendency in the material to stretch rather than rupture under impact actions.

To clarify the concepts, each first attenuated zone (6) is per definition delimited by the locations (102)  
15 where the thickness of ply A (or ply D) as indicated by arrows is the average between the smallest thickness in this zone and the highest thickness in the adjacent non-bonded zone.

Structures with "first attenuated zones" as shown in  
20 Figs. 2 to 5 and structures with both "first and second attenuated zones", as shown in Figs. 3 can also be produced with machinery which make transverse fluting. This shall be described later.

In Fig. 6 both plies A and B are in themselves  
25 laminates, for instance cross-laminates as in claim 22, and each film from which the plies are produced is co-extruded. Therefore A and B are each formed by a lamination process (the "pre-lamination") prior to the lamination of A to B. Layer (1) is the main layer in each of the two coex films  
30 which make A, and layer (2) is the main layer in the two coex films which make B. Layers (1) and (2) can e.g. consist of high density polyethylene (preferably HMWHDPE) or iso- or syndio-tactic polypropylene (PP) or blends of one of these polymers with a more flexible polymer, for  
35 instance, for HMWHDPE, LLDPE. If stiffness is the most preferred property of the minifluted laminate, plain HMWHDPE or plain PP may be chosen, but if tear and puncture

properties play a more important role and/or superior heat-seal properties are essential, the mentioned blends may be more suited.

Layers (3) are coextruded surface layers with the  
5 function to improve the heat-seal properties of the finished, minifluted laminate and/or modify its frictional properties. Layers (4) are co-extruded surface layers ("lamination layers") with the two functions: a) to facilitate the pre-lamination and b) to control the bonding  
10 strength (in cross-laminates the bonding should not be too strong, otherwise the tear propagation strength suffers).

Similarly, layers (5) are co-extruded surface layers to facilitate the lamination of the entire A to the entire B and control the strength of the bonding between A and B.

15 With reference to Fig. 7 and Fig. 8 the structure shown in Fig. 2 can be formed by passing film (A) first over the grooved pre-heating roller (6a) which heats it only along the lines which shall become attenuated, then over the grooved stretching rollers (7) and (8), further  
20 over grooved transfer and flute-stabilizing roller (9), and finally over grooved lamination roller (10) and its rubber-coated counter-rollers (11), while film (B) is passed over the smooth rollers (12) and (11). The grooves of all of the rollers are circular so that the flutes are formed in  
25 the machine direction. If B is transversely oriented and therefore has a tendency to transverse shrinkage, rollers (12) and (11) are preferably supplied with devices, e.g. belts, to hold the edges (not shown). All of these rollers are temperature controlled rollers, rollers (9), (10), (11)  
30 and (12) being controlled at the lamination temperature, rollers (6a) and (8) at a somewhat lower temperature and roller (7) at a temperature about 20 or 30°C. (There can be further rollers for preheating of B). By choice of suitable, coextruded surface layers - see (5) in Fig. 6 -  
35 the lamination temperature is kept far below the melting range of the main layers in (A) and (B). The temperature of the zones (6) in (A) during the transverse stretching

between rollers (7) and (8) is preferably still lower, e.g. in the range of about 50-70°C and the rest of (A) much lower, e.g. around room temperature, as it also appears from the mentioned roller temperatures. If the main layers in (A) and (B) consist of plain HDPE or blend of HDPE and LLDPE, the lamination temperature is preferably chosen between about 80 and about 110°C, and the coextruded lamination layers, which can consist of a suitable plain or blended copolymer of ethylene, are chosen to produce lamination at this temperature.

The crests on roller (8) has very small radius of curvature, e.g. about 0.05mm or an extremely narrow "land". The crests on roller 6a which have the function to preheat, may, depending on the film, be similar or somewhat rounder or with a slightly wider land. The crests on rollers (7) and (9) have a higher radius of curvature or a wider land, to avoid transverse stretching on these crests. Suitable values for the sizes of the grooves are mentioned below in the example.

The different temperatures on the different grooved rollers cause different thermal expansions, compared to a state where all have room temperature, and this must be taken into consideration when the grooved rollers are constructed, since they must fit exactly to each other during operation. (10°C heating of a 10cm long steel roller segment causes about 0.011mm expansion of this segment). Reference is again made to values in the example.

Rollers (7), (8) and (10) are driven, while rollers (6a), (9), (11) and (12) may be idling.

As it will be understood, the attenuation of A in the zones (6) takes place almost entirely by the transverse orientation at a temperature essentially below the melting range of the main body of A. This attenuation therefore does not cause any significant weakening of A's transverse strength, contrarily it will normally cause an increase of this strength. After the transverse stretching on the

crests of roller (8) the width of the "first attenuated zones" (6) should preferably not exceed (as a rule of the thumb) half the wavelength, but the degree of stretching should normally be as high as practically obtainable, while  
5 the degree of transverse stretching between the "first attenuated zones" normally should be as low as practically obtainable, with the intended result that ply A in the unbonded zones becomes as thick as the chosen square metre weight of A allows and the flutes become as high as  
10 possible.

A practical way of achieving that the first attenuated zones and the zones of bonding match with almost equal width is the following: the relatively flat crests on the laminating roller (10) are made slightly wider than the  
15 chosen width of the first attenuated zones, and the temperature and velocities are adjusted to each other in such a way that the first attenuated zones (6) become heated to a temperature at which the material will laminate with B, while the thicker A-ply between zones (6) does not  
20 reach a temperature at which lamination can take place.

The use of longitudinally oriented A-ply as in claim 6 will impart a tendency in A to "neck down" and form thin longitudinal lines when A is stretched transversely. Therefore, longitudinally oriented A-ply will enhance the  
25 possibilities of getting a sharp distinction between strongly attenuated zones (6) and non-attenuated ply A between these zones.

Theoretically there will always occur some attenuation also of the B-ply in the zones of bonding, since the  
30 bonding is established under pressure, but this attenuation has no positive effect and should preferably not exceed 20%. Due to the presence of lamination layers (see (5) in Fig. 6) such attenuation of the B-ply can be made negligible.

35 In Fig. 8 the minifluted laminate leaving lamination rollers 10 and 11 is marked (B/A), In this figure it proceeds for lamination in conventional manner with the

non-waved, mono-/or multilayered film C coming from the smooth steel roller (13). The lamination takes place between the smooth steel rollers (14) and (15) of which at least roller (14) is heated to a convenient lamination temperature and is driven. The waved film A is heated to lamination temperature, at least on its free crests, by means of hot air from the blower (16). Rollers (14) and (15) are kept at a distance from each other which is small enough to effect the lamination but big enough to avoid excessive flattening, e.g. between 0.2 and 0.6mm. When A, B and C are very thin films, e.g. each in the range of 0.03-0.10mm thick (for A this refers to the non-waved form) such conventional lamination would have been very difficult due to the floppiness of waved A, but since the flutes now have been consolidated by the bonding to B, the lamination of A to C presents no particular difficulty.

The laminate leaving the lamination rollers (14) and (15) is marked B/A/C. It is cooled, e.g. by air (not shown) and may normally be reeled up or flip-flopped, since it normally is sufficiently flexible material although fluted, or it may directly be cut into lengths.

To make the laminate shown in Fig. 5, one option is to make the A/B laminate shown in Fig. 2, and laminate this over the rollers (11) and (10) with the fluted ply D leaving roller (9). This requires exact registration between the rollers which make the A/B laminate and roller (1)). Alternatively B can consist of e.g. two films B1 and B2. Then in two mutually independent processes there are made an A/B1 laminate and a D/B2 laminate, and the two are bonded together with B1 against B2 in an extrusion lamination process.

With certain modification the line shown in Figs. 7 and 8 can also be used to make the laminate of Fig. 3, which has "second attenuated zones". For this purpose roller (6a) should have the same surface profile and the same low temperature as roller (7), and it should be preceded by and in slight engagement with a roller with the



same surface profile as roller (8), which roller should have the same higher temperature as roller (8).

In the minifluted "multi-crosslaminate" shown in Figs. 9a, 9b and 9c, the two coextruded films (1a) and (1b) from which A is made by "pre-lamination", are oriented in criss-crossing directions, which form an angle lower than 45° with the longitudinal direction (the flute direction) as symbolized by the arrows (1aa) and (1bb). This gives a resultant main orientation direction for A parallel with the flute direction, symbolized by the arrow marked A'. Similarly the two coextruded films (2a) and (2b) from which B is made by "pre-lamination", are oriented in criss-crossing directions, which form an angle higher than 45° with the flute direction, as symbolized by the arrows (2aa) and (2bb). This gives a resultant main orientation direction of B perpendicular to the flute direction, symbolized by the arrow B'.

In Fig. 10a, which as mentioned shows a longitudinal section through a flute in ply A, the latter has been flattened and sealed to ply B at intervals (103) to form pockets or "mini-containers", and these mini-containers have been filled with a particulate substance (104) which has a purpose for the use of the laminate, e.g. for protection of material packed or wrapped up in the latter. As one among many options it may be an oxygen scavenger. To enhance the action of the substance the flutes may be supplied with fine perforations on the side towards the packed product. The substance may also e.g. be a fire retardant material such as  $\text{CaCl}_2$  with crystal water, or just fine sand to increase the bulk density of the laminate.

Fig. 11 which shall be described below, shows how the particulate substance can be fed into the flutes of ply A prior to its lamination with ply B, and how the flutes can be closed to pockets by transverse sealing after the lamination, without any essential contamination of these transverse seals.

A laminate between a fluted thermoplastic film and a non-fluted thermoplastic film with a filling material between is known from Japanese Patent publication No. 07-276547 (Hino Masahito). However, in this case the filling material is a continuous porous sheet (for absorption) which extends from flute to flute without interruptions, so that there is no direct bonding between the flute and the non-fluted films. One of the thermoplastic films is first directly extruded unto this porous (e.g. fiberformed) sheet, then the two together are given a fluted shape between gear rollers while the thermoplastic film still is molten, and finally a second thermoplastic film is extruded directly unto this fluted assembly to join with the porous sheet. Hereby the bonding necessarily must be very weak, and the mechanical characteristics must be completely different from those of the present product. The wavelength of the fluting is not indicated.

In the technical filter material for liquid or gas flows shown in Fig. 10b there is inserted a strand or yarn into each flute - in connection with the description of Fig. 11 it shall be explained how that can be done - and both sides of each channel formed by fluted ply A and non-fluted ply B is supplied with a row of perforations, (106) in ply A and (107) in ply B. These rows are mutually displaced as shown so that the liquid or gas passing from one surface of the laminate to the other, is forced to follow a channel over a distance corresponding to the displacement. The fitting between the yarn and the channel may be improved by shrinkage of A and/or B after the lamination process.

The pocket structure shown in Fig. 10a can also be used for filtration purposes if ply A and ply B are supplied with mutually displaced holes. Then the particulate substance (104) can e.g. consist of active charcoal, or an ion-exchange resin, or for simple filtration purposes fine sand. Also in this case a

tightening of the passage by means of shrinkage can be advantageous or may even be essential.

Practical examples of the use of such filter materials are for air filtration systems including absorption of  
5 poisonous substances, and ion-exchange processes. In both cases the laminate can have the form of a long web which is slowly advanced transversely to the flow which passes through it.

Another practical use is as a substitute of  
10 geotextiles e.g. for road constructions. Such textiles must allow water to penetrate but hold back even fine particles. The present laminate, e.g. filled with fine sand in the pockets, is suitable for this use.

For such filtration purposes, high puncture strength  
15 will often be needed, and the laminate then preferably comprises oriented, cross-laminated films.

For the filtration purposes the condition that the wavelength should not exceed 3mm, is often less important since appearance and handle may not be a primary concern as  
20 it is in the case of laminates for ordinary tarpaulin uses.

The weather protective laminate shown in Fig. 10c, e.g. for raincoats, also has a pocket structure, whereby ply A is heat-sealed to ply B by transverse seals at locations (103), but there is no particulate substance in  
25 the pockets. Like the laminate for filtration, each line of pockets is supplied with perforations in a displaced system, here shown as groups of perforations (109) in A and similar groups (110) in B, and these groups are mutually displaced. In this sketch it is considered that ply A is  
30 on the side where it rains, and a person, animal or item, which the laminate shall protect, is on the ply B side. (It could be the other way round). It is also considered that the direction shown by arrow (108) is upward. Since the perforations (109) are at the bottom of the pockets,  
35 and because of the gravity force, only the bottom of the pockets may be filled with rainwater, while in principle no water will reach the perforations (110). On the other hand

there is free passage of air and transpiration between the hole groups (109) and (110). Also in this product the wavelength may to some extent exceed 3 mm.

The modification of the Fig. 8 machine-line, which is  
5 shown in Fig. 11, is adapted to fill a particulate substance (104) into the channels formed between A and B. The filling is here shown very schematically. The powder (104) is taken from a hopper (111) and is administered by means of an adjustable vibrator (not shown). It falls into  
10 the fluted ply A at the upper side of the grooved lamination roller (10). At regular time intervals hopper (111) is filled up with the powder (104). The means for this are not shown. Other conventional systems for administering the powder (104) onto ply A on roller (10)  
15 may of course be chosen.

Roller (10) vibrates (means not shown) so that the powder is moved from the higher zones, i.e. those which become bonded zones when A meets B in the nip between (10) and (11), into the lower zones, which become the "channels".

20 Having left the laminating rollers (10) and (11). The A+B- laminate with powder (104) in the channels moves towards the cog-roller (113) - its surface is shown in a detailed part-drawing - and its rubber-coated counter-roller (114) which together flatten and close the channels  
25 by making transverse seals. Roller (113) is vibrated in order to remove powder away from the channel-parts which become flattened and sealed.

Both rollers (113) and (114) are heated to a temperature needed for the sealing, and since the laminate  
30 while entering these rollers still is at about a temperature suitable for heat-sealing due to the previous temperatures, this second heat-seal process needs not cause a deceleration of the entire process.

Ply A and/or ply B may be perforated by means of pin-  
35 rollers after rollers (10)/(11) and in front or after the pair of rollers (113)/(114). In case mutually displaced rows of perforations are needed (see Figs. 10b and c) and

pin-rollers for ply A and ply B must be suitably coordinated, and in case the perforations should have a fixed relation to the transverse seals (see Fig. 10c, the pin-rollers must be coordinated with roller (113).

5        In order to make the product shown in Fig. 10a, rollers (113) and (114) are omitted or taken out of function, and instead of administering powder into ply A, there is at the same place laid a yarn into each flute. Each yarn is taken from a separate reel.

10        At some stage after rollers (10)/(11), ply A and/or ply B may be subjected to transverse shrinkage. If this is done with ply A only, it may be sufficient to heat the ply A-side of the laminate to an adequate temperature by means of hot air or on one or more hot rollers. If ply B  
15        should be involved in the shrinkage it may be necessary to hold the laminate at the edges while it shrinks. This may be done by means of an ordinary tenterframe, but the latter should be set up to work "inversely" so that the width gradually is reduced instead of increased.

20        The methods applied for making pockets from the flutes, fill powder into these flutes, and making suitable perforations, have been explained in connection with the longitudinally fluted laminate. Analogous methods can be applied in connection with a transversely fluted laminate  
25        (the general method of making such laminate appears from Fig. 12), and in that case the closing of the channels to form pockets may take place by use of a circularly or helically grooved roller. However, it is not considered practically possible to lay down yarn in transverse flutes  
30        at industrially acceptable velocities.

      The process for making the transversely fluted laminate, which appears from the flow-sheet Fig. 12 is generally analogous to the process which is described in connection with Figs. 7 and 8, and the profiles of the  
35        grooved rollers can also be generally similar, except that for the process of Fig. 12 the grooves extend axially, while for the process of Figs. 7 and 8 they are circular.

Step 1: Ply A is longitudinally stretched in very narrow zones localized on the tips of a hot roller which has a profile similar to that of roller (8). The grooved counter-roller, which is cold, has a profile like that of roller (7).

Step 2: The warm, stretched "second attenuated zones" are cooled on a cold grooved roller which also has a profile like that of roller (7), and then to form "first attenuated zones" between the "second", ply A is longitudinally stretched between this cold roller and a warm grooved roller which also has a profile similar to that of roller (8). The stretching is localized to the tips of this roller. Similar to the registration in printing technology, step 2 is brought in registration with step 1 under use of a device which optically detects the stretched zones.

Step 3: The flutes are first formed in the grooves of a hot roller with a profile similar to that of roller (10), e.g. under use of compressed air, and are held in the grooves e.g. under use of a vacuum, all as explained in connection with Fig. 13, and ply A is then laminated with ply B between the crests of this grooved roller and a rubber-coated counter-roller, which also is heated. Ply B has been preheated.

There can be different after treatments as explained in the foregoing.

In Fig. 13, ply A which has been supplied first with the very narrow transverse "second attenuated zones" (101), and then with the somewhat wider, also transverse "first attenuated zones" (6), is directed into the grooves (115) of the heated lamination roller by means of compressed air from a row of nozzles of which one (116) is shown. By use of registration means, working on basis of optical detection of zones (6) or (101) it is arranged that the first attenuated zones (6) will cover the crests (118) of the grooved roller. The two sets of attenuated zones act as hinges so that even a quite heavy ply A may be bent and

form the flutes. The latter are held in shape in the grooves under use of vacuum applied through channels (117) from the interior of the roller. Thus ply A is moved in flute shape to the nip (not shown) between the grooved roller and the rubber-coated counter-roller, where lamination takes place. The vacuum in the grooves is adjusted so that ply A is held firmly when this is needed, but can be released where that is needed. There can also be a valve arrangement inside the grooved roller to eliminate the vacuum during the release.

#### Example

A 2-ply laminate of fluted ply A and non-fluted ply B with A longitudinally and B transversely oriented is manufactured on a pilot-unit constructed as shown in Figs. 7 and 8, but terminating after the lamination of A and B have taken place. Both plies consist of one coextruded, cold-stretched 0.037mm thick film consisting of HDPE with a thin layer on one side, consisting of an ethylene copolymer having a melting range between 95-105°C. This is used as lamination layer in the process. The cold-stretching was carried out near room temperature at a draw ratio about 3:1 and was followed by heat stabilization, all by conventional means, and while the film had flat tubular form. The tube was longitudinally cut to form ply A.

Processes for continuous manufacture of transversely oriented film are well-known and mentioned in the foregoing, but it would have caused practical complications for the inventor to have such film manufactured according to his specifications, and therefore short lengths of the ply A-film were glued together edge to edge with a pressure-sensitive adhesive to form a transversely oriented web.

All of the grooved rollers have the pitch 1.1000mm at the temperature at which they actually are used, but due to the large temperature differences during the stretching/laminating process, the thermal expansion had to be taken into consideration when these rollers were

machined at 20°C, see the table below. The biggest temperature difference between the rollers, as it appears from this table, is 85°, and this corresponds to an expansion of about 0.10mm per 10 cm roller length, while the accumulated error in the fitting between adjacent rollers from end to end of the rollers must be maintained lower than 0.15mm to obtain the needed registration.

The table below also indicates the radius of curvature (R) or the length of a "land" on the crest of each grooved roller, as seen in the axial section in Fig. 7.

Roller No.	6a	7	8	9	10
Crest	land	R=	land	R=	Land
15 mm	0.4	0.2	0.15	0.15	0.7
Temperature °C	70	20	70	105	105
20 Pitch mm	1,0993	1,1000	1,0993	1,0988	1,0988

It is of course not practically possible to achieve such a high accuracy in the pitch seen individually from groove to groove, but it is essential that errors in the pitch do not accumulate by more than 0.05mm. This is best achieved when the surface parts are made from segments and accumulated errors are eliminated by fine grinding of the segment ends and/or thin shims (foils) are inserted between the segments. In the actual pilot machine the length of the grooved part of each roller surface was about 450mm and was assembled from 3 segments. It is judged that in an industrial machine the rollers can be made in up to about 5 m length, but in that case the accuracy from end to end has to be checked with laser measurements and adjustments made as explained.



The transverse stretching, which is the basis for the flute-formation and which forms the "first attenuated zones" - later the zones which become bases, not crests of the flutes in the laminate - takes place by the intermeshing between rollers (7) and (8) and becomes localized to a zone on and nearby the crests of roller (8). This is because roller (8) is hot and has a relatively sharp crest, while roller (7) is cold and has a much rounder crest (higher radius of curvature R). It is relevant also in this connection that ply A is uniaxially oriented in the machine direction and therefore has a high tendency to "neck-down" and form sharply delimited attenuated zones when it is transversely stretched.

The function of roller (6a) is to preheat the zones which are to be stretched on the tips of roller (8). In this example the "land" on the crests of roller (6a) are wider than the "land" on the crests of roller (8). This has been chosen in order to counteract the very pronounced tendency in the film to "neck-down", in other words, to make the limits of the "first attenuated zones" smoother. In other cases e.g. when ply A has a pronounced transverse orientation and therefore no tendency to "necking down" by transverse stretching, the "land" on the crests of roller (6a) which preheats the film, should be no wider than the "land" on the crests of roller (8).

Between rollers (6a) and (7) there is a slight but almost zero engagement to avoid wrinkles without stretching the films.

Having left the transverse stretching roller (8), ply A is taken over by transfer roller (9). This is heated in order to help the shaping of flutes in the zones which have not been stretched. At this stage the "first attenuated zones" are still deeply curved, but when (A) is taken over by the flat 0.4mm wide crests (lands) on the grooved laminating roller (10) the "first attenuated zones" are flattened almost over their entire width except at their boundaries where the thickness gradually increases, and by

means of the rubber-coated counter-roller, which on its surface has temperature 80°C, this flat portion is laminated to the transversely oriented ply B.

Prior to the experimental run the axial position of  
5 the grooved rollers are very carefully adjusted to each other, and so is the intermeshing between adjacent grooved rollers. The intermeshing between rollers (7) and (8) is set to make the depth of the fluting 0.40mm, as measured in microscope on a cross-section of the finished laminate.

10 When leaving the stretching/laminating apparatus, the minifluted laminted is aircooled and is reeled up on a core of diameter 250mm. In the test report below this laminate is called "Sample I".

It is noted that although the pitch of each grooved  
15 roller in the line is 1,1000mm referring to the temperature at which the roller has been operated, the wavelength of the fluting in the final minifluted laminate, due to transverse shrinkage, is only 1.0mm.

As a principal experiment there is out specimens of  
20 this film, 30cm long in the machine direction and 20cm wide in the transverse direction, and these specimens are subjected to further transverse shrinkage by a primitive arrangement which imitates an "inverse" operation of a tenter frame. The two 30cm long edges are fixed to two  
25 sticks, which are held by hand, and an even shrinkage is arranged by moving the specimen over a roller surface, which is heated to 115°C, with the B film contacting the roller. Hereby the wavelength is reduced from 1.0mm to 0.8mm.

30 Sample II, made for comparison: By a relatively primitive arrangement there is made specimens of corrugated board material from the same film as used to make "Sample I" (coextruded coldstretched HDPE-film of thickness 0.037mm), with all dimensions of sample A, namely as  
35 follows:

Surprisingly samples (I) and (II) show the same stiffness, namely 1.6 gram per mm, while sample (III) shows 0.13 gram per mm, in other words the present invention has magnified the stiffness in one direction by a factor of about 12, as measured by this method.

It should have been expected that sample (III) would have shown higher stiffness than sample (I). When this is not the case, the explanation probably is that the flutes may have been pressed relatively flat right from the beginning of the depression, although in elastic manner.

In the characterisation of the product and method of the invention, it has been emphasised that the wavelength of the fluted ply A or the pitch on the grooved laminating roller should be no more than 3mm in order to give the corrugated laminate the character of a flexible film rather than a board material. However, in connection with the description of the filter material, in which liquid or gas passes from holes in one ply to displaced holes in the other ply, and on the way passes a filler, it was nevertheless stated that for such purposes the wavelength may exceed the 3mm. Similar is true for the described weatherprotective corrugated laminate, in which there also are displaced holes, but usually no filler, and the gravity force is used to "filter" the rainwater from the passing air.

Furthermore, the making of "first attenuated zones" and optionally also "second attenuated zones" has been explained as useful measures for obtaining the "miniflutes", be it in connection with longitudinally or transversely fluted laminates. Since these zones act as "hinges" - see e.g. Fig. 13 - they enable for a given thickness of ply A a finer wavelength and/or deeper fluting than it otherwise could be achieved. In the foregoing there has also been stated other useful effects of the "first attenuated zones" and the "second attenuated zones", and it is clear that similar advantages can be achieved

Sample	Wavelength mm	Bonded Zones mm	Flute-depth mm
I	1.0	0.4	0.4
II	5.5	2.2	2.2

It is noted that II's wavelength, 6.0mm, is slightly less than the minimum mentioned in patent literature namely in US-A-4.132.581.

In both samples I and II, the direction of orientation in ply A is parallel with the flutes, and the direction of orientation in B is perpendicular to the flutes.

Sample B is manufactured with a small laboratory machine constructed as explained in connection with Fig. 13, but in this case there has now been any need to make "first attenuated zones" and "second attenuated zones". The flutes become perpendicular to the machine direction. Like the grooved laminating roller (10) used in the manufacture of sample I, this grooved laminating roller is heated to 105°C.

Sample III, made for comparison: The same film (coextruded oriented HDPE, 0.037mm thick) is crosslaminated with itself without any fluting being made.

Comparisons between samples I, II and III:

Appearance and handle:

(II) looks and feels like a board material, but is instable when bent or compressed between the fingers.

(I) has a rather textilis look, can stand a substantial amount of bending and compression between the fingers without changing its character, and it has a feel of "bulk".

Bending tests:

(I) and (II) are bent over cylindrical bodies of different diameters, and it is examined how small that diameter can be before the flutes begin to collapse in a non-elastic manner, i.e. so that there remain marks in the flutes after the specimen has been straightened out again.

(II) can withstand bending down to a diameter of 250mm, while (I) can withstand bending down to a diameter of 50mm.

#### 10 Stiffness measurements:

10cm long specimens are cut out from samples (I), (II) and (III).

The specimens from sample (I) each comprises 20 flutes and at the edges a bonded zone. The width of these specimens is 21mm.

The specimens from sample (II) each comprise 4 flutes and at the edges a bonded zone. The width of these specimens is 23mm.

The width of each sample (III) specimen is 21mm.

20 For controlled bending of the specimens there is made a very lightweight support arrangement comprising two supports with 50mm spacing between. This support arrangement is placed on the table of a letter balance. The bending is effected by means of a cylinder which has a diameter 50mm and starts pressing at the middle of the supported sample. This cylinder is assembled on a stand and can be moved up and down. Corresponding values of the depression in mm and the resisting force in grams are measured and plotted. Up to a certain limit there is a linear dependence, and from the declination of the line and stiffness is calculated as grams force per mm depression. In order to obtain reliable reading for sample (III), 10 specimens are laid one on top of the other. The value of stiffness is determined for this bunch and divided by 10.

35

#### Results

Surprisingly samples (I) and (II) show the same stiffness, namely 1.6 gram per mm, while sample (III) shows 0.13 gram per mm, in other words the present invention has magnified the stiffness in one direction by a factor of  
5 about 12, as measured by this method.

It should have been expected that sample (III) would have shown higher stiffness than sample (I). When this is not the case, the explanation probably is that the flutes may have been pressed relatively flat right from the  
10 beginning of the depression, although in elastic manner.

In the characterisation of the product and method of the invention, it has been emphasised that the wavelength of the fluted ply A or the pitch on the grooved laminating roller should be no more than 3mm in order to give the  
15 corrugated laminate the character of a flexible film rather than a board material. However, in connection with the description of the filter material, in which liquid or gas passes from holes in one ply to displaced holes in the other ply, and on the way passes a filler, it was  
20 nevertheless stated that for such purposes the wavelength may exceed the 3mm. Similar is true for the described weatherprotective corrugated laminate, in which there also are displaced holes, but usually no filler, and the gravity force is used to "filter" the rainwater from the passing  
25 air.

Furthermore, the making of "first attenuated zones" and optionally also "second attenuated zones" has been explained as useful measures for obtaining the "miniflutes", be it in connection with longitudinally or  
30 transversely fluted laminates. Since these zones act as "hinges" - see e.g. Fig. 13 - they enable for a given thickness of ply A a finer wavelength and/or deeper fluting than it otherwise could be achieved. In the foregoing there has also been stated other useful effects of the  
35 "first attenuated zones" and the "second attenuated zones", and it is clear that similar advantages can be achieved

when the wavelength of the product or the pitch of the grooved lamination roller exceeds 3mm.

Therefore the product and the making of the "first attenuated zones" and optionally and "second attenuated  
5 zones" placed as it has been described in the foregoing, is considered an invention independently of the wavelength.

## Claims

1. Laminate comprising at least a monofilm formed or multifilm formed ply (A) and another monofilm formed or multifilm formed ply (B) both mainly consisting of thermoplastic polymer material, whereby at least A consists of cold-orientable material in which A has a waved flute configuration while B is not waved, and B on a first side is adhesively bonded in bonding zones to the crests on a first side of A, characterised in that the wavelength ( $\lambda$ ) of the said configuration is no more than 3mm, that the adhesive bonding has been established through a lamination layer, and in that either the thickness of A is generally the same within the non-bonded zones as it is within the bonded zones, or A exhibits first solid-state-attenuated zones extending parallel to the flute direction, each bonding zone mainly being located within a said first attenuated zone whereby each said first attenuated zone is understood as delimited by the positions where the thickness is an average between A's lowest thickness within the first attenuated zone and A's widest thickness within the adjacent non-bonded zone.
2. Laminate according to claim 1, characterised in that the ply A by the choice of polymer material or by an incorporated filler or by orientation, within the non-bonded zones exhibits an average yield tension parallel to the direction of fluting, which at an extension velocity of  $500\% \text{ min}^{-1}$ , is no less than  $30 \text{ Nmm}^{-2}$ , preferably no less than  $50 \text{ Nmm}^{-3}$  and still more preferably no less than  $75 \text{ Nmm}^{-2}$ .
3. Laminate according to claim 1 or claim 2 characterised in that the wavelength of each flute including an adjacent bonding zone is no longer than 50 times the highest thickness of A within the flute, preferably no more than 40 times and still more preferably no more than 30 times the said thickness.
4. Laminate according to any preceding claims characterised in that the width of each bonding zone is no



less than 15% preferably no less than 20% and still more preferably no less than 30% of the wavelength.

5. Laminate according to any of the preceding claims characterised in that the width of the non-bonded zone of  
5 A as measured between the two adjacent bonding zones and measured along its curved surfaces is no less than 10% and preferably no less than 20% longer than the corresponding linear distance.

6. Laminate according to any of the preceding claims  
10 characterised in that A, within each non-bonded zone and outside the first attenuated zone if such zone is present, is molecularly oriented mainly in a direction parallel to the direction of the flutes or in a direction close to the latter as determined by shrinkage tests.

15 7. Laminate according to claim 6, characterised in that B also is molecularly oriented and B's orientation within each non-bonded zone in a direction perpendicular to the direction of the flutes is higher than A's average orientation in the same direction within the non-bonded  
20 zone, the said two orientations being determined by shrinkage tests.

8. Laminate according to claims 6 or 7, characterised in that the yield tension in A in a direction parallel with the flutes and the yield tension in B in a direction  
25 perpendicular to the flutes, both referring to the cross-section of the respective ply and determined in the non-bonded zones on narrow strips at an extension velocity of  $500\% \text{ min}^{-1}$ , is no less than  $30 \text{ Nmm}^{-2}$ , preferably no less than  $50 \text{ Nmm}^{-2}$  and still more preferably no less than  $75$   
30  $\text{Nmm}^{-2}$ .

9. Laminate according to any of the preceding claims, characterised in that B has a lower coefficient of elasticity than A, both as measured in the direction perpendicular to the flute direction.

35 10. Laminate according to claim 7, characterised in that the choice of B and of depth of fluting is so that by stretching of the laminate perpendicular to the direction

of the fluting up to the point where the waving has disappeared, B still has not undergone any significant plastic deformation, preferably B is selected as a thermoplastic elastomer.

- 5 11. Laminate according to any of the preceding claims, characterised in that it comprises at least two films which each has a main direction of orientation and which are laminated so that the said two directions cross each other.
- 10 12. Laminate according to any of the preceding claims, in which said first attenuated zones are present in A characterised in that each such zone of attenuated A, if it extends beyond the corresponding zone of bonding into a non-bonded zone of A, is limited to a width which leaves more than half of and preferably no less than 70% of the
- 15 width of the non-bonded zone, as not belonging to any first attenuated zone, this width being measured along the curved surfaces.
- 20 13. Laminate according to claim 12, characterised by a second solid-state-attenuated zone (hereinafter the second attenuated zone) between each pair of adjacent first attenuated zones said second attenuated zones being narrower than said first attenuated zones and located on the crests of A.
- 25 14. Laminate according to any of the preceding claims, characterised in that the wavelength of A is no more than 2.5mm, preferably no more than 2mm and more preferably no more than 1.5mm.
- 30 15. Laminate according to any of the preceding claims, characterised in that it comprises a further non-waved monofilm formed or multifilm formed ply (C) of thermoplastic polymer material, C being bonded to the crests of A on the second side of the latter through a lamination layer.
- 35 16. Laminate according to any of the preceding claims characterised in that it comprises a further monofilm formed or multifilm formed ply (D) consisting of thermoplastic, cold-orientable polymer material, said ply

having waved flute configuration, the crests on one side of D being bonded to the second side of B through a lamination layer, and the wavelength of D's flute configuration preferably being no more than 3mm.

- 5 17. Laminated according to any of the preceding claims, characterised in that at least some of the flutes are flattened at intervals and preferably bonded across each ones entire width at the flattened locations to make the flute form a row of narrow closed elongated pockets.
- 10 18. Laminate accordingly to claim 17, characterised in that the flattened portions of a number of mutually adjacent flutes or of all flutes form a series of lines transverse to the longitudinal direction of the flutes.
- 15 19. Laminate according to any of the preceding claims, characterised in that the bonding of the crests on A, is effected through selected surface layers formed in a co-extrusion process.
- 20 20. Laminate according to any of the preceding claims, characterised in that the mono- or multifilm formed plies mainly consist of polyolefin.
- 25 21. Laminate according to claim 12, characterised in that said first attenuated zones of A are attenuated so that the minimum thickness in that zone is less than 75% of the maximum thickness of A in the non-bonded zone, preferably less than 50% and more preferably less than 30% of that maximum thickness.
- 30 22. Laminate according to any of the preceding claims, characterised in that A and B each has a main direction of orientation, either by being uniaxially oriented or unbalanced biaxially oriented, or by in itself being a cross-laminate of uniaxially oriented or unbalanced biaxially oriented films, such cross-laminate exhibiting a resultant main direction of orientation, whereby the resultant main direction of orientation in A is generally
- 35 parallel with the longitudinal direction of the flutes, while the resultant main direction of orientation in B forms an angle to the said direction in A.

23. Laminate according to claim 15, characterised in that B and C each has a main direction of orientation, either by being uniaxially oriented or unbalanced biaxially oriented, or each in itself being a cross-laminate of uniaxially or  
5 unbalanced biaxially oriented films, said cross-laminate exhibiting a resultant main direction of orientation whereby the main direction of orientation in B criss-crosses the main direction of orientation in C.

24. Laminate according to claim 23, characterised in that  
10 A in a non-oriented state exhibits a co-efficient of elasticity E which is lower than E of both B and C in non-oriented state, preferably by a factor of at least 1.5 and more preferably at least 2.

25. Laminate according to claim 24, characterised in that  
15 the flutes are flattened at intervals and bonded across each ones entire width to make the flute form a row of narrow closed pockets.

26. Laminate according to any of claims 1 to 22 characterised in that by the choice of polymer material or  
20 by an incorporated filler or by orientation, the co-efficient of elasticity E in Ply A measured in the unbonded zone in the direction parallel to the flute as an average over the unbonded zone is no less than 700 MPa, and preferably no less than 1000 MPa.

27. Laminate according to any of the preceding claims, characterised in that at least some of the channels formed by the flutes and the matching non-waved film material, which channels may be closed to pockets, contain a filling material in particulate, fibrous, filament or liquid form.

28. Laminate according to claim 27, characterised in that  
30 said material is a preservative for goods intended to become packed in or protected by the laminate, preferably an oxygen scavenger or ethylene scavenger, a biocide, such as a fungicide or bactericide, a corrosion inhibitor or a fire extinguishing agent, optionally with perforations  
35 established in the flutes or non-waved film material to enhance the effect of said preservative.

29. Laminate according to claim 27, characterised in that said filling material consists of reinforcement yarn or reinforcement filaments.

5 30. Laminate according to claim 27, characterised in that said filling material is adapted to act as a filter material by holding back suspended particles from a liquid passing through the channels or pockets or is an absorbent or ion exchanger capable of absorbing or exchanging matter dissolved in such liquid, said filler optionally being  
10 fibre-formed or yarn-formed, and that each filled flute and matching non-waved film material is supplied with a row of perforations, whereby the perforations or groups of perforations in a flute and the perforations or groups of perforations in the matching non-waved film material are  
15 mutually displaced so as to force the liquid with the suspended particles, while passing from one surface of the laminate towards the other surface, to run through the filter material in a direction parallel to the longitudinal directions of the flutes.

20 31. A bag made from the laminate according to claim 1, characterised in that the laminate comprises only the two mono- or multifilm formed plies A and B, and in that the bottom and top of the bag are generally perpendicular to the longitudinal direction of the flutes.

25 32. A self-standing bag or pouch made from the laminate according to claim 1, in which the bottom of the bag or pouch is gusseted, and front and back faces of the bag or pouch are adhesively joined at their edges preferably by heat-sealing, characterised in that the laminate comprises  
30 only the two mono- or multifilm formed plies A and B, and in that the bottom and top of the bag or pouch are generally parallel with the longitudinal direction of the flutes.

33. A self-standing bag or pouch according to claim 32,  
35 characterised in that the capability of the bag or pouch to stand on its own is enhanced by flat-pressed lines

generally perpendicular to the longitudinal direction of the flutes.

34. Geotextile substitute capable of letting water through but withholding the soil, constructed according to  
5 claim 30 and preferably comprising oriented and cross-laminated films.

35. Geotextile substitute accordingly to claim 34, characterised in that the filler is sand.

36. Method of manufacturing a laminate or monofilm formed  
10 or multifilm formed ply (A) with another monofilm formed or multifilm formed ply (B) both consisting of thermoplastic polymer material in which A has a waved flute configuration while B is not waved, and B on a first side is adhesively  
15 bonded in zones to the crests on a first side of A, in which further the waved flute structure is formed by the use of a grooved roller, and the said bonding with B is carried out under heat and pressure and also under use of a grooved roller, and at least A is selected as mainly consisting of solid-state orientable material,  
20 characterised in that the division on the grooved roller which produces the lamination on the said crests is at the highest 3mm.

37. Method according to claim 36, characterised in that  
25 prior to the said bonding process A is solid-state stretched in narrow zones to form first attenuated zones which are parallel to the selected direction of fluting, said stretching being generally perpendicular to the said direction and carried out between a set of grooved rollers both different from the grooved roller for lamination, and  
30 that the grooved roller for lamination is coordinated with the said set of grooved roller for stretching in such a way that each zone of bonding mainly becomes located within a first attenuated zone.

38. Method according to claim 37, characterised in that  
35 prior to or after the formation of the first attenuated zones another set of grooved rollers produces second attenuated zones which is another series of solid-state

oriented narrow zones in A, parallel with the first attenuated zones and narrower than the latter, and the grooved rollers which produce said second attenuated zone are coordinated with the grooved rollers which produce the first attenuated zones so that there is produced a second attenuated zone generally in the middle between each two neighbours of second attenuated zones.

39. A method according to any of claims 36 to 38, characterised in that the division of the grooved roller which produces the lamination on the crests is at the highest 2.5mm, preferably no more than 2.0mm and still more preferably no more than 1.5mm.

40. A method according to any of claims 36 to 39, characterised in that prior to the forming of the waved flute structure and if the methods of claims 37 and/or 38 are used, also prior to the formation of the attenuated zones, the film or films which constitute A are supplied with orientation in one or both directions, the resultant main direction of orientation being in the direction which is selected to become the direction of fluting.

41. Method according to any of claims 36 to 40, characterised in that simultaneously with or subsequent to the bonding of B to A a further non-waved monofilm formed or multifilm formed ply (C) of thermoplastic polymer materials is adhesively bonded to the crests of A on the second side of the latter.

42. Method according to any of claims 36 to 40, characterised in that in a manner similar to the forming and application of A there is produced a second monofilm formed or multifilm forms ply (D) having waved flute configuration with a wavelength preferably of no more than 3mm, and the crests on one side of D are laminated to the second side of B simultaneously with or following the lamination of B with A.

43. Method according to any of the claims 36-42, characterised in that the mono- or multi-film formed plies,

mainly consist of polyolefin, and are produced by a process involving extrusion.

44. Method according to any of claims 36 to 43  
5 characterised in that the films constituting the plies are made by co-extrusion in which there are co-extruded surface layers to enable the lamination without any melting of the main body of the films.

45. Method according to any of claims 36 to 44  
10 characterised in that after the said lamination at least some of the flutes are flattened in locations placed at intervals, preferably under heat and pressure sufficient to bond all films in the laminate to each other in said locations so that the flutes with adjacent film material form fine elongated pockets.

15 46. Method according to claim 45, characterised in that said flattening is carried out with bars or cogs which have their longitudinal direction arranged transversely to the flute direction and each covering a number of flutes, optionally the entire width of the laminate.

20 47. Method according to any of claims 37 to 46 characterised in that a suitably distinct stripe formation of the first attenuated zones is established at least in part by giving the crests on the grooved stretching roller intended to produce the stripes a temperature which is  
25 higher than the temperature of the crests on the other grooved stretching roller and/or by giving the crests on the grooved stretching roller intended to produce the stripes a radius of curvature which is smaller than the radius of curvature of the crests on the matching grooved  
30 stretching roller.

48. Method according to any of claims 36 to 47  
characterised in that particulate, liquid or thread/yarn-formed material is filled into some at least of those  
flutes in A which, by the lamination to B, are closed to  
35 form channels, this filling taking place before, prior to or during said lamination.



49. Method according to claim 48, characterised in that after filling the filled channels are closed at intervals by pressure and heat to form filled pockets.

50. Method according to any of claims 48 to 49,  
5 characterised in that prior to, simultaneously with or following the filling step perforations are made in the laminate at least on one side to help the filling material or part thereof dissipate into the surroundings or to allow air or liquid to pass through the pack of filling material.

10 51. Method according to claim 50, characterised in that there is made a row of micro perforations on each side of each filled channel, said rows being mutually displaced to force air or liquid which passes through the laminate to run a distance along a channel or pocket.

15 52. Method according to any of claims 36 to 51, characterised in that B prior to the lamination is supplied with orientation generally perpendicular to the direction which becomes direction of fluting, and after the lamination B is subjected to shrinkage in a direction  
20 generally perpendicular to the direction of fluting.

53. Method according to any of claims 36 to 52, characterised in that the waved flute structure is established essentially in A's longitudinal direction under a generally transverse orientation process by taking A  
25 through a set of driven mutually intermeshing grooved rollers, the grooves on the rollers being circular or helical and forming an angle of at least 60° with the roller axis.

54. Method according to claim 53, characterised in that  
30 A is passed directly from its exit from one of the grooved stretching rollers which form the waving on A to the grooved lamination roller, these two grooved rollers being in close proximity to each other and having the same pitch when measured at each ones operational temperature and  
35 being mutually adjusted in the axial direction.

55. Method according to claim 53, characterised in that A is passed from its exit from one of the grooved

stretching rollers which form the waving on A to the grooved lamination roller over one or a series of heated, grooved transfer rollers, the grooved rollers in the row starting with the grooved stretching rollers and ending  
5 with the grooved lamination roller each being in close proximity to its neighbour or neighbours, whereby each of the grooved rollers in the row has the same pitch when measured at their respective operational temperature, and being mutually adjusted in the axial direction.

10 56. Method according to any of claims 36 to 52 characterised in that each grooved roller used to form the flutes in A and A to B, and each grooved roller used to form the first attenuated zones according to claim 37 if such zones are produced, and each grooved roller used to  
15 form the second attenuated zones according to claim 38 if such zones are formed, is a grooved roller in which the grooves are essentially parallel with the roller axis, and means are provided to hold the flutes of A in the grooves in the roller on which these flutes are formed and bonded  
20 during the passage from the position where the flutes are formed to the position where A is bonded to B, said holding means adapted to avoid a frictional rubbing on A during said passage.

57. Method according to claim 56, characterised in that  
25 the flutes in A are formed by use of an air jet or a transverse row of airjets which directs A into the grooves on the forming roller.

58. Method according to claims 56 or 57, characterised in that  
30 that if first attenuated zones are formed accordingly to claim 37 by grooved rollers acting in coordination with the grooved roller used for lamination, said coordination consists in an automatic fine regulation of the relative velocities between the rollers.

59. Method according to claim 58, characterised in that  
35 when second attenuated zones are formed according to claim 38 by grooved rollers acting in coordination with the grooved rollers used to produce the first attenuated zones,

said coordination consists in an automatic fine regulation of the relative velocities between the rollers.

60. Method according to claim 36, characterised in that the bonding is established through a lamination layer.

5 61. Laminate according to claim 22, characterised in that there is only the two mono- or multilayered films A and B and A is unoriented states exhibits a co-efficient of elasticity E which is lower than the E exhibited by B in unoriented state, preferably by a factor of at least 1.5  
10 and more preferably by a factor of at least 2.

62. A laminate according to any of the claims 1-26 made to be weather (rain and wind) resistant and air-permeable, characterised in that at least some of the channels formed either by waved ply A and non-waved ply B and/or C and/or  
15 waved ply D are connected to the environment on both sides of the laminate through perforations, the perforations on the two sides of a channel being mutually displaced so as to force air or water which pass through the laminate to run a distance through a channel.

20 63. Laminate according to any of the preceding product claims, characterised in that there is print on A and/or B in the non-bonded zones, the bonded zones being generally devoid of such print.

64. Method according to any of the preceding method  
25 claims, characterised in that A and/or B is printed on the surface to become the inside of the laminate, the printing process being in register with the flute-forming and lamination processes so as to limit the print generally to the non-bonded zones.

30 65. Apparatus for forming a laminate comprising feeding means for feeding a continuous web of ply B formed of a thermoplastic material from a supply to a laminating station;

a grooved fluting roller for imposing a waved fluted  
35 structure on a ply of thermoplastic material;

feeding means for feeding a continuous web of ply A formed of a thermoplastic material from a supply to the

grooved fluting roller and thereafter to the laminating station in face to face relationship with ply B;

wherein the laminating station comprises a grooved laminating roller which is capable of applying heat and pressure between the crests of the flutes of ply A and ply B so as to bond the contacting surfaces of ply A and ply B in bonding zones to form a laminate product;

characterised in that the division between the crests of the laminating roller is no more than 3mm.

66. Apparatus according to claim 65 comprising a pair of intermeshing grooved stretching rollers for solid-state stretching of ply A in a direction substantially perpendicular to the flutes upstream of the laminating roller, to form first attenuated lines mutually separated in said perpendicular direction, the grooves of the stretching rollers being adapted and aligned with those of the laminating roller so that each bonding zone is located mainly within a first attenuated zone.

67. Apparatus according to claim 66 in which the apparatus comprises heating means for heating ply A in discrete zones destined for stretching to form the first attenuated zones, said means preferably comprising a heated grooved roller positioned so as to allow contact of the heated tips of the grooves with ply A upstream of the pair of grooved stretching rollers, in line with the grooves of the stretching rollers.

68. Apparatus according to claim 66 or 67, in which the radius of curvature of the tips of the grooves of at least one of the stretching rollers, any heating means, the speed of transport of ply A and the extent of intermeshing of the rollers are adapted so as to attenuate the thickness of ply A in the attenuated zones to a thickness that is less than 75% of the original thickness of ply A, preferably less than 50% of the original thickness and more preferably less than 30% of the original thickness.

69. Apparatus according to any of claims 66 to 68 in which the radius of curvature of the tips of the grooves of

at least one of the stretching rollers, any heating means, the speed of transport of ply A and the extent of intermeshing of the rollers are adapted so as to provide an attenuated zone which extends beyond the bonded zone for no more than x% of the linear width between adjacent bonded zones. [This is meant to correspond to claim 12)

70. Apparatus according to any of claims 66 to 69 comprising a pair of second intermeshing grooved stretching rollers for solid-state stretching of ply A in a direction substantially perpendicular to the flutes upstream of the laminating roller, to form second attenuating zones mutually separated in said perpendicular direction, the grooves of the second stretching rollers being adapted and aligned relative to the grooves of the laminating roller so that the second attenuated zones are located between the first attenuated zones whereby a second attenuated zone is located between each adjacent pair of first attenuated zones.

71. Apparatus according to claim 70 in which the pair of second stretching rollers are separate from the pair of first stretching rollers.

72. Apparatus according to any of claims 66 to 71 in which the fluting rollers comprises the or each grooved stretching roller pair.

73. Apparatus according to any of claims 65 to 72 in which the division  $\lambda$  between the crests of the laminating roller is no more than 2.5mm, preferably no more than 2.0mm, more preferably no more than 1.5mm.

74. Apparatus according to claim 73 in which the grooves of the laminating roller have substantially flat crests having a width in the range  $(0.15 \text{ to } 0.9) \lambda$ , preferably in the range  $(0.2 \text{ to } 0.8) \lambda$ , more preferably  $(0.3 \text{ to } 0.75) \lambda$ .

75. Apparatus according to any of claims 65 to 74 in which the grooved laminating roller applies heat and pressure on the plies A/B against a flat counter-roller, preferably having a rubbery surface.

76. Apparatus according to any of claims 65 to 75 comprising grooved transfer rollers between the fluting roller(s) and the laminating roller whereby ply A remains in contact with the surface of at least one grooved roller from the upstream fluting roller to the laminating station.

77. Apparatus according to any of claims 65 to 76 in which the grooves of each grooved roller are circular.

78. Apparatus according to any of claims 65 to 76 in which the grooves of each grooved roller are parallel to the roller axes.

79. Apparatus according to any of claims 65 to 78 comprising means for supplying the A/B laminate from the laminating station to a downstream C ply laminating station;

means for supplying a continuous web of substantially smooth ply C formed of a thermoplastic material from a supply to the second laminating station so as to be in face to face relationship with the A/B laminate and in contact with A.

wherein the second laminating station comprises rollers for applying pressure between ply C and the A/B laminate to bond A to C.

80. Apparatus according to claim 79 comprising means for heating the surface of A of the A/B laminate and/or the face of C brought into contact with the A/B laminate prior to or simultaneously with application of pressure in the C-ply laminating station.

81. Apparatus according to any of claims 65 to 80 comprising a grooved ply D fluting roller for imposing a waved fluted structure on a ply D of thermoplastic materials;

feeding means for feeding a continuous web of ply D formed of thermoplastic material from a supply to the grooved ply D fluting roller and thereafter to a ply D laminating station;

means for supplying ply B to the ply D laminating station for face to face contact of ply D with ply B on the

side of B opposite to the side in face to face contact with A,

wherein the ply D laminating station comprises a grooved ply D laminating roller for applying heat and pressure between ply D and the crests of ply D in ply D bonding zones so as to bond the contacting surfaces in the said ply D bonding zones.

82. Apparatus according to claim 81 wherein the division between the grooves of the ply D laminating roller  $\lambda_D$  is the same as  $\lambda$  and the ply D bonding zones are directly opposite the bonding zones of A and B.

83. Apparatus according to any of claims 65 to 82 comprising a printing station for printing an ink onto a surface of ply A and/or ply B, preferably in register with the fluting and laminating rollers, preferably onto a surface of a ply destined to be an internal surface in the laminate product.

84. Apparatus according to any of claims 65 to 83 comprising a flute flattening station for imposing pressure on the laminate of A and B at intermittent positions along at least one flute, preferably for providing a continuous flattened zone transverse to the direction of the flutes across the entire width of the laminate in which the contacting faces of the plies are adhered to one another to form closed pockets.

85. Apparatus according to any of claims 65 to 84 comprising a bag forming station for forming bags or pouches from the laminate product by heat sealing side and/or bottom and/or top seals of face to face arranged laminates.

86. Apparatus according to 85 in which the bag forming station forms gusseted bags with gusseted bottoms and heat-sealed sides, and in which the bottoms are parallel with the flutes.

87. Apparatus according to any of claims 65 to 84 comprising perforating means for perforating ply A and/or ply B of the laminate downstream of the said laminating

station, the perforating means being aligned with the laminating roller whereby the plys are perforated between the bonded zones.

88. Apparatus according to any of claims 65 to 87  
5 comprising a filler station between the fluting roller(s) and the laminating roller for introducing filling material into the flutes between ply A and ply B.

89. Apparatus according to claim 88 in which the filler material is in particulate, fibrous or yarn form.



Fig.1.

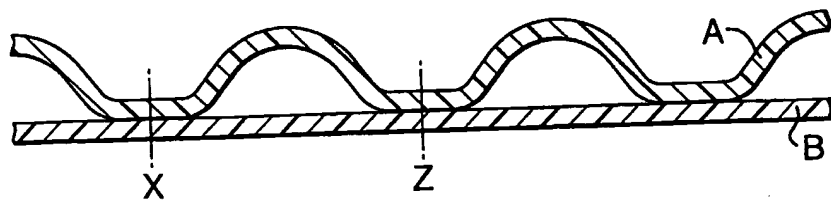


Fig.2.

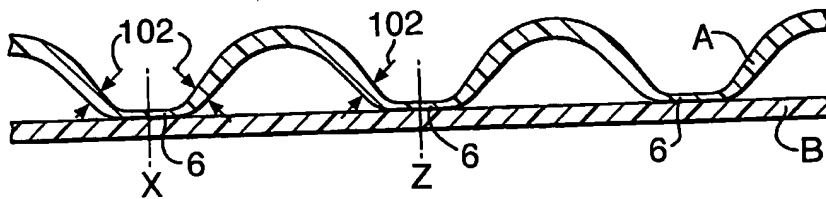
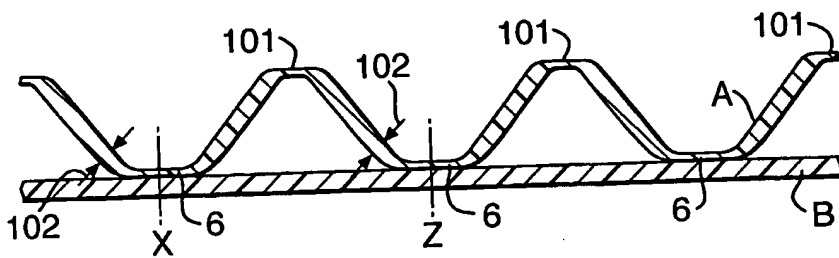


Fig.3.



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Fig.4.

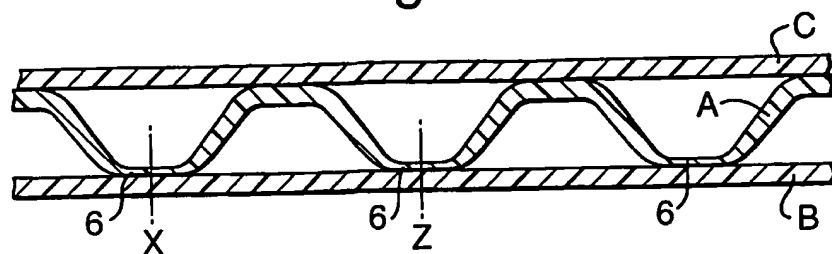


Fig.5.

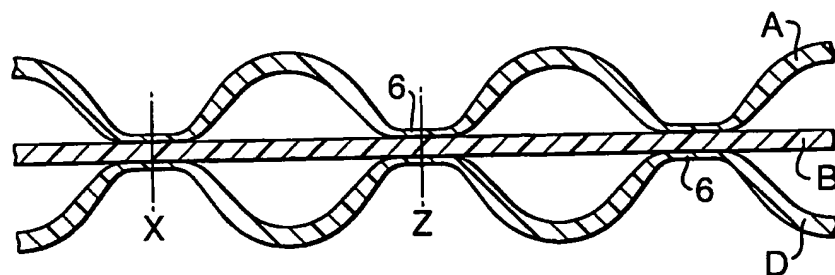


Fig.6.

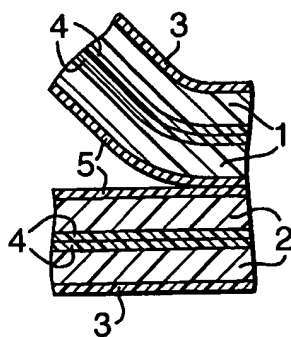
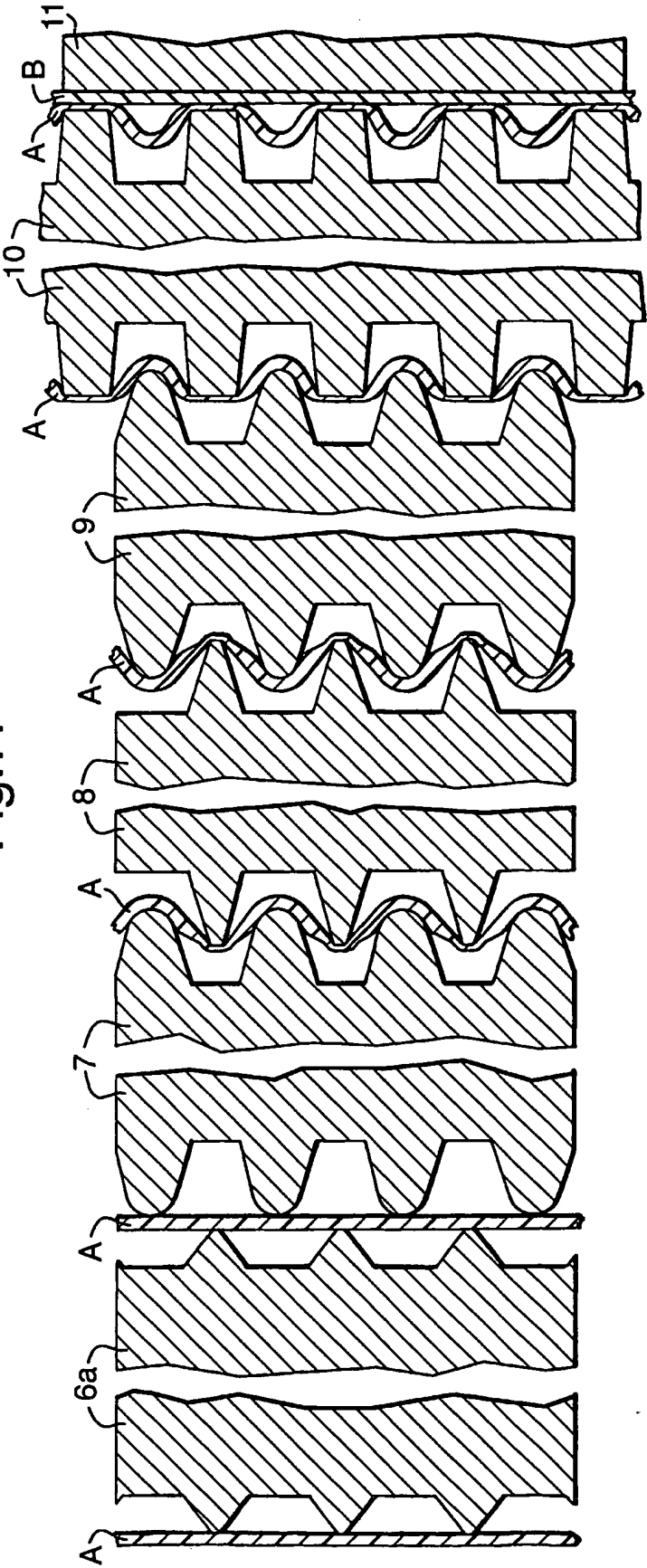


Fig.7.



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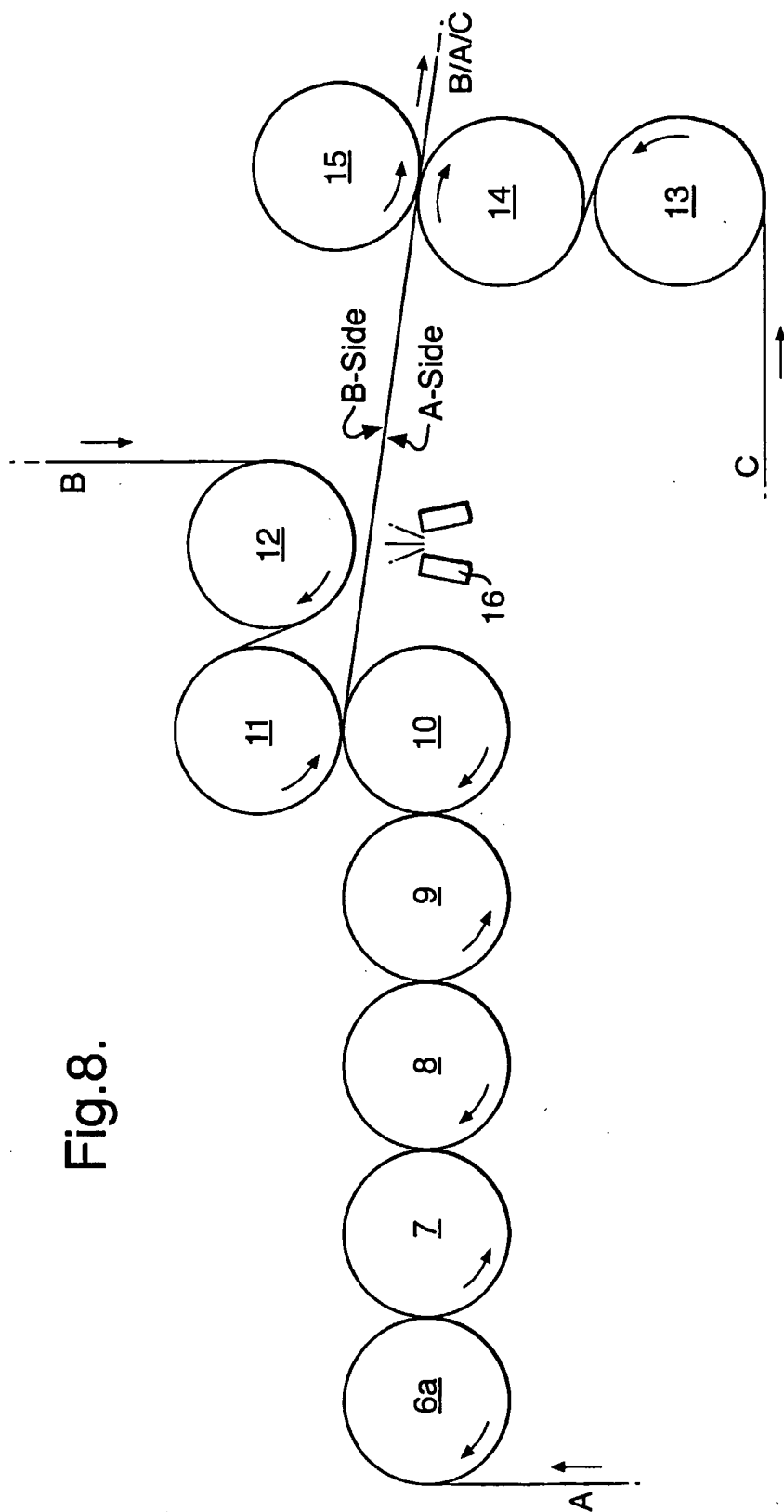


Fig.8.

Fig.9a.

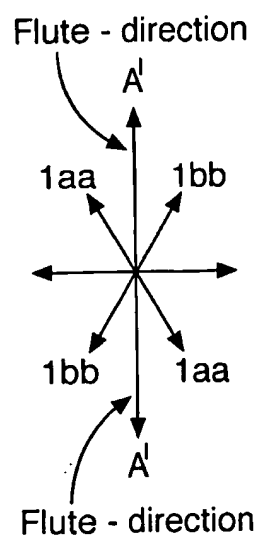


Fig.9c.

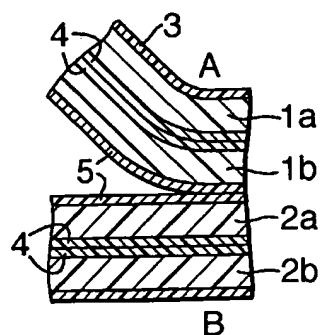


Fig.9b.

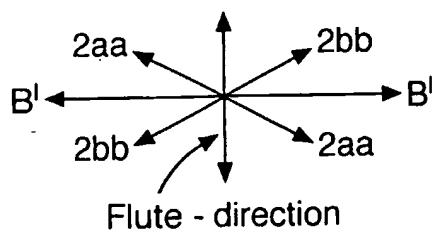


Fig.10a.

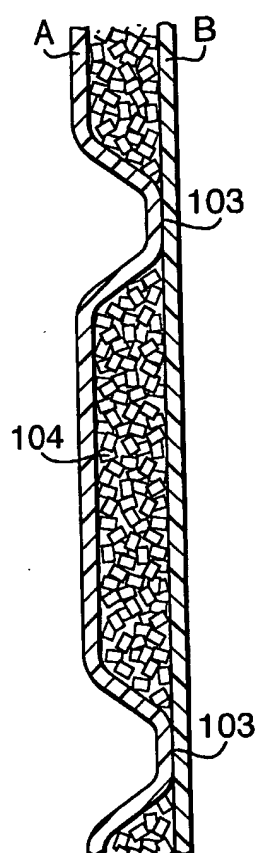


Fig.10b.

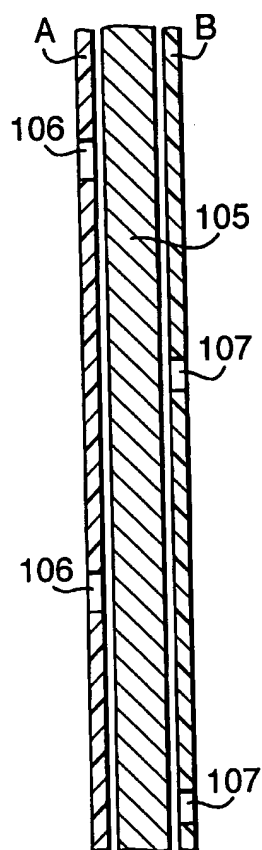
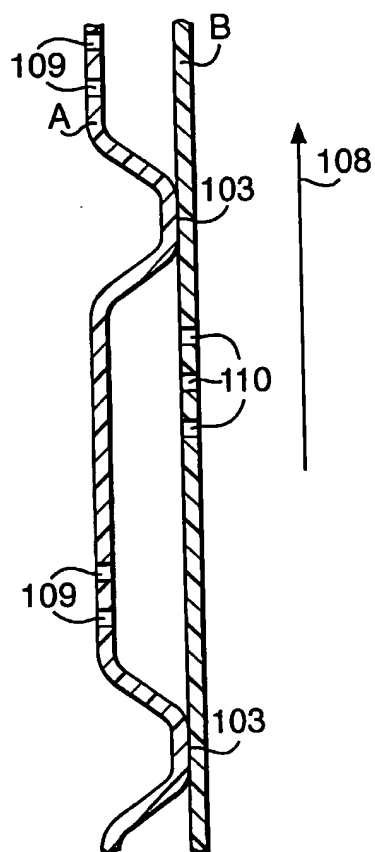


Fig.10c.



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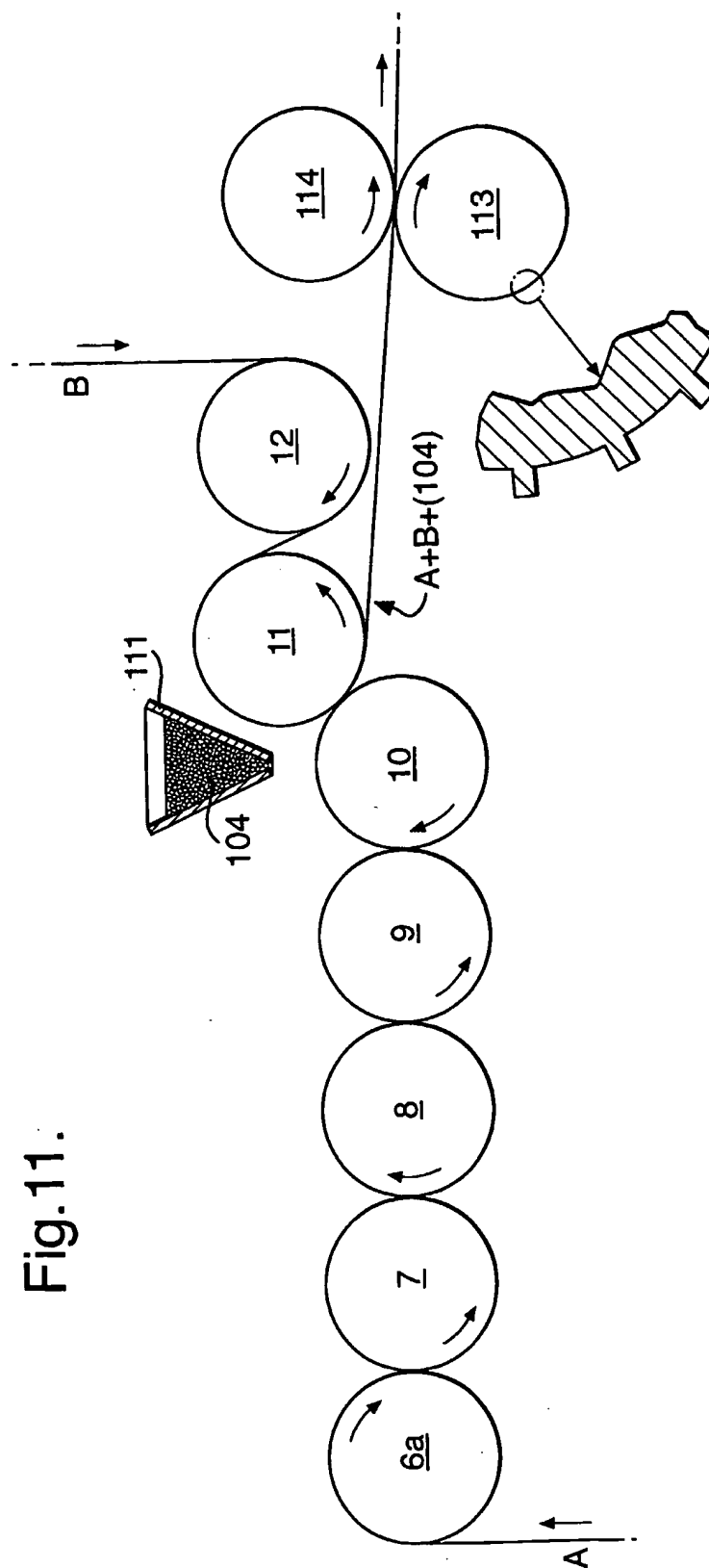


Fig.11:

Fig.12.

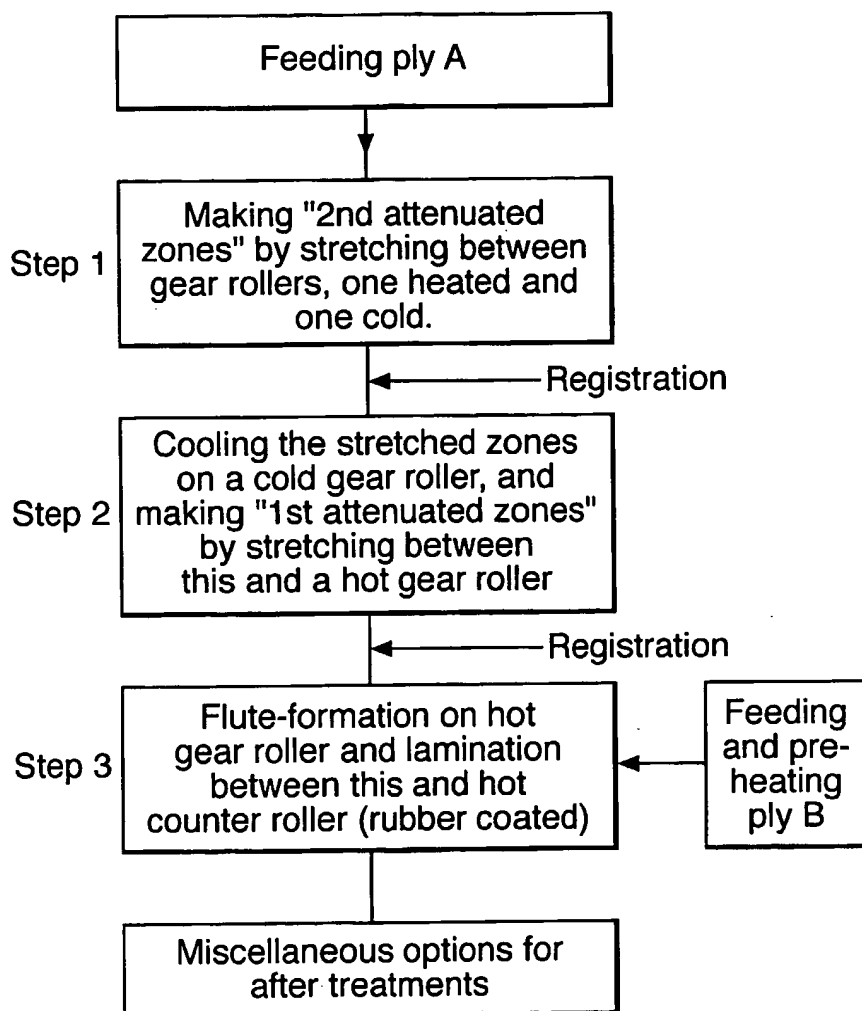
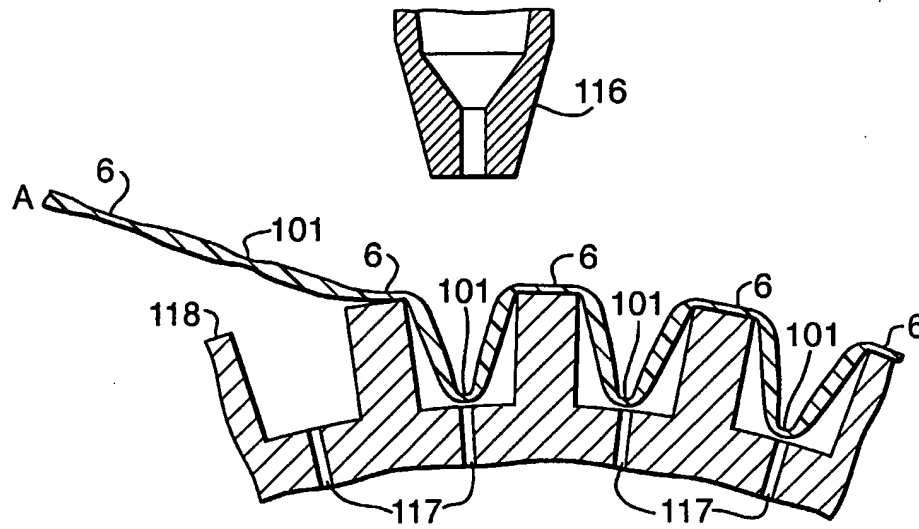




Fig.13.



<b>A. CLASSIFICATION OF SUBJECT MATTER</b> IPC 7    B32B27/00    B32B27/32    B32B3/28    B65D65/40		
According to International Patent Classification (IPC) or to both national classification and IPC		
<b>B. FIELDS SEARCHED</b> Minimum documentation searched (classification system followed by classification symbols) IPC 7    B32B    B65D		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched		
Electronic data base consulted during the International search (name of data base and, where practical, search terms used) EPO-Internal, WPI Data, PAJ		
<b>C. DOCUMENTS CONSIDERED TO BE RELEVANT</b>		
Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 4 132 581 A (SWARTZ HENRY D) 2 January 1979 (1979-01-02) cited in the application claims 1,3 column 1, line 56 -column 2, line 68 column 6, line 61 -column 7, line 2 column 9, line 63 -column 10, line 20 example 1 ---	1-89
A	WO 94 05489 A (MCGRATH STEPHEN EDWARD) 17 March 1994 (1994-03-17) claims 1,3,4,7,8,14 page 2, line 10 -page 3, line 18 page 6, line 35 -page 7, line 8 -----	1-89
<input type="checkbox"/> Further documents are listed in the continuation of box C. <span style="margin-left: 100px;"><input checked="" type="checkbox"/> Patent family members are listed in annex.</span>		
* Special categories of cited documents : <div style="display: flex; justify-content: space-between;"> <div style="width: 45%;"> <p>*A* document defining the general state of the art which is not considered to be of particular relevance</p> <p>*E* earlier document but published on or after the international filing date</p> <p>*L* document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>*O* document referring to an oral disclosure, use, exhibition or other means</p> <p>*P* document published prior to the international filing date but later than the priority date claimed</p> </div> <div style="width: 45%;"> <p>*T* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>*X* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone</p> <p>*Y* document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.</p> <p>*&amp;* document member of the same patent family</p> </div> </div>		
Date of the actual completion of the international search <div style="text-align: center; font-weight: bold; margin-top: 10px;">31 October 2002</div>		Date of mailing of the international search report <div style="text-align: center; font-weight: bold; margin-top: 10px;">07/11/2002</div>
Name and mailing address of the ISA European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Tx. 31 651 epo nl, Fax: (+31-70) 340-3016		Authorized officer <div style="text-align: center; font-weight: bold; margin-top: 10px;">Ibarrola Torres, O</div>

Patent document cited in search report		Publication date	Patent family member(s)		Publication date
US 4132581	A	02-01-1979	US	4188253 A	12-02-1980
WO 9405489	A	17-03-1994	CA	2070077 A1	01-12-1992
			WO	9405489 A1	17-03-1994